

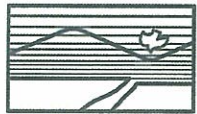
# MASTER PLAN HYDROLOGY REPORT



PREPARED FOR:

## SOUTH SHORES CHURCH CITY OF DANA POINT

PREPARED BY:



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DATE PREPARED:

February 29, 2012

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## **I. INTRODUCTION**

The proposed project involves the redevelopment of the existing South Shores Church site that spans an area of approximately 6 acres which consists primarily of a parking lot area and four (4) buildings including an existing preschool, administration / fellowship hall, chapel, and sanctuary. The property is located in the area north of the Pacific Coast Highway (PCH) on Crown Valley Parkway in the City of Dana Point with a site address of 32712 Crown Valley Parkway.

The redevelopment will be performed in phases to replace the older preschool, administration, and chapel buildings. The sanctuary building will be maintained on the site. A parking structure, which a part of is subterranean, is also proposed as part of the redevelopment to accommodate projected parking demands.

## **II. REPORT SCOPE**

The purpose of this report is to establish both existing and post development peak flows of the site through hydrologic analysis and to identify potential issues and associated mitigations in regards to storm run-offs and water quality, as part of the Conditional Use Permit (CUP) phase of the project. Since the site will be constructed in phases, it is necessary within this report to convey the extreme (or site build-out) conditions as indicated herein. Any phased storm drain construction within the confines of the site shall be addressed during the permitting of each phase with a separate grading plan and amendments to this preliminary hydrology. Further refinements of the discharge rates will be visited at each phase of the design but the objective to limit potential post development off-site peak discharge to existing values as established herein shall be maintained.

It should be noted that a hydrology study by Norris Repke dated February 23, 2007 was initially prepared for this project. However, subsequent revisions of the hydrology study shall be performed by Adams-Streeter Civil Engineers, Inc.

## **III. METHODOLOGY**

The hydrology calculations were performed in accordance with the requirements of the Orange County Hydrology Manual. The rational method calculations were developed utilizing Advanced Engineering Software (AES). The 25-year frequency and 100-year frequency storm calculations are located in the Appendix. The project site has soil with hydrologic classifications of principally Type "D".

#### **IV. EXISTING CONDITIONS**

The existing site of approximately 6.0 acres has been previously developed and is currently occupied by a preschool, administration / fellowship hall, chapel, sanctuary building with supporting surface parking facilities. There is permanent landscaping throughout the site consisting of trees and shrubs including native type vegetation along the man-made and natural slopes that bound the site along the easterly property boundary. The watershed is classified as a non-mountainous area. The slope of the existing site terrain is substantially uniform with the existing parking lot sloping at approximately 2.5% to 4%. The terrain behind the existing buildings on the easterly edge slopes at approximately 3 (horizontal) to 1 (vertical) and generally comprises of shrubbery and trees.

The parking lot sheet flows in a south-easterly direction to a single catch basin that intercepts and conveys surface flows to an on-site underground storm drain which outlets onto an off-site man-made open channel that almost immediately drains into an outlet structure. Both the off-site channel and outlet structure are located adjacent to the south-easterly corner of the property. Other portions of the site also drain to the parking lot and follow the same path to the existing outlet structure. The remainder portions of the site drain towards the existing slopes along the easterly and northeasterly edge of the site. The drainage patterns as described are illustrated on the Existing Drainage Area Exhibit and the Existing Condition Hydrology Map included in the Appendix.

The existing outlet structure was originally constructed in the early 1990's as a temporary retarding basin. The original intention was that this temporary facility would be removed and storm drain facilities would be extended as a part of a proposed housing development. However, the housing development did not occur and the area adjacent to the outlet structure is now an open-space area which will not be developed.

The outlet structure is a shallow basin formed by low earthen berms with outlet pipes. A small volume of water is periodically retained within the outlet structure basin but only for short durations due to discharge through the outlet drains and the action of percolation and evaporation. There is an existing perforated pipe riser within the basin of the outlet structure that meters flows to an existing concrete "v-ditch". Only flows up to the rates of low frequency storms are delivered to the "v-ditch" because of the small diameter of the riser and limited head available to deliver flows to the ditch. The "v-ditch" carries flows in a southerly direction and also collects flows from the housing project to the south of the Church. An overflow pipe embedded in the berm of the outlet structure also provides for any potential overflow to be discharged to grade during higher frequency storms. There are signs of limited erosion along the open space path of this flow.

The outlet structure accepts drainage from the church property and has been serving as an erosion control measure which dissipates the energy of high velocity flows resulting from the upstream on-site underground pipe that runs down a 3:1 slope.

The Church has a recorded easement that encompasses the outlet structure and has been periodically cleaning the outlet structure to minimize vegetation overgrowth and to remove

refuse deposits. A copy of the recorded easement agreement is in the appendix of this report.

The temporary basin was designed to decrease peak flows coming from the property to the original flows that occurred before the construction of the main sanctuary building. These original flows were calculated in the Hydrology and Hydraulic Report for South Shores Baptist Church, prepared by David A. Boyle Engineering on January 10, 1991. The hydrology report calculated that the 100-year peak flow being discharged by the property and outletting at the south-east corner was equal to 12.33 cfs. This accounted for approximately 3.2 acres of the property's total 6.0 acres. The report also included calculations that proved the existing concrete v-ditch, which is the ultimate conveyance structure, was able to meet capacity. See Appendix for original calculations prepared by Boyle Engineering.

After the sanctuary building was constructed, the property's peak discharge increased. These peak discharge numbers have been calculated in this report and are referred to as "Existing Conditions". While the peak flows calculated for the existing conditions are larger than the original flows calculated by Boyle Engineering, the temporary basins acted as a detention basin which reduced the discharge to the existing v-ditch.

The original design of the basin included three in-line basins with outlet pipes as described above. Since the construction of the church sanctuary, 2 of the 3 basins no longer exist. While no significant signs of overflow or erosion can be seen, it is assumed that the remaining basin is undersized and will not be able to handle the needed capacity for larger storm events. For this reason, it is the intent of this report to eliminate the basin and replicate pre-existing flows as calculated by the Boyle Engineering Hydrology Report.

## **V. PROPOSED CONDITIONS**

In its ultimate condition the project will be developed as shown on the Proposed Master Site Plan (Architectural Plan A3.0) which is included in the Appendix. The majority of the proposed site, Area "A", is comprised of approximately 4.0 acres. To reduce peak flows, flows from Area "A" will enter a proposed underground detention system. This underground detention system will be comprised of two 84" pipes with a restrictor plate at its outlet. The location of the underground detention system is shown on the Developed Condition Hydrology Map. This proposed storm drain will continue to collect flows from Area "B" downstream of the detention system before discharging to the existing concrete v-ditch at the property's south-east corner. A discharge head wall and v-ditch connection will have to be constructed to properly convey flows from Areas "A", "B", and "C" to the existing v-ditch.

The proposed underground temporary-detention basin will reduce the site's developed peak flow to match existing flows as calculated by the Boyle Engineering Hydrology report. The balance of the site that does not enter the storm drain system, shown as Area "D" is considered natural slope. These peak flows are reduced substantially, as shown in Table A-1. Area "E", comprised of driveways, sidewalk and parkway, sheet flows towards Crown Valley

Parkway and is also reduced from existing conditions. A copy of the Developed Condition Hydrology Map that shows the concept drainage system is included in the Appendix.

**TABLE A-1**

LOCATION	AREAS		25-YEAR PEAK FLOW		100-YEAR PEAK FLOW	
	EXISTING (ACRES)	DEVELOPED (ACRES)	EXISTING (CFS)	DEVELOPED (CFS)	EXISTING (CFS)	DEVELOPED (CFS)
"A", "B", & "C"	3.2	5.2	13.1 / 9.6*	8.9	16.8 / 12.3*	10.0
"D"	2.4	0.7	11.3	2.8	14.3	3.6
"E"	0.4	0.1	1.7	0.4	2.1	0.6

*\*Flows refer to existing peak flows as calculated by the Hydrology Report prepared by Boyle Engineering.*

The Drainage Area Exhibits in Section VIII show the relationship between the existing and developed conditions. The amount of flows being re-directed away from the slope at the north-easterly property is significant and should be considered beneficial to the slope stability of that area. While the acreage increases for Area "A", "B", & "C" in the developed condition, the proposed on-site detention system significantly reduces the site's peak flow.

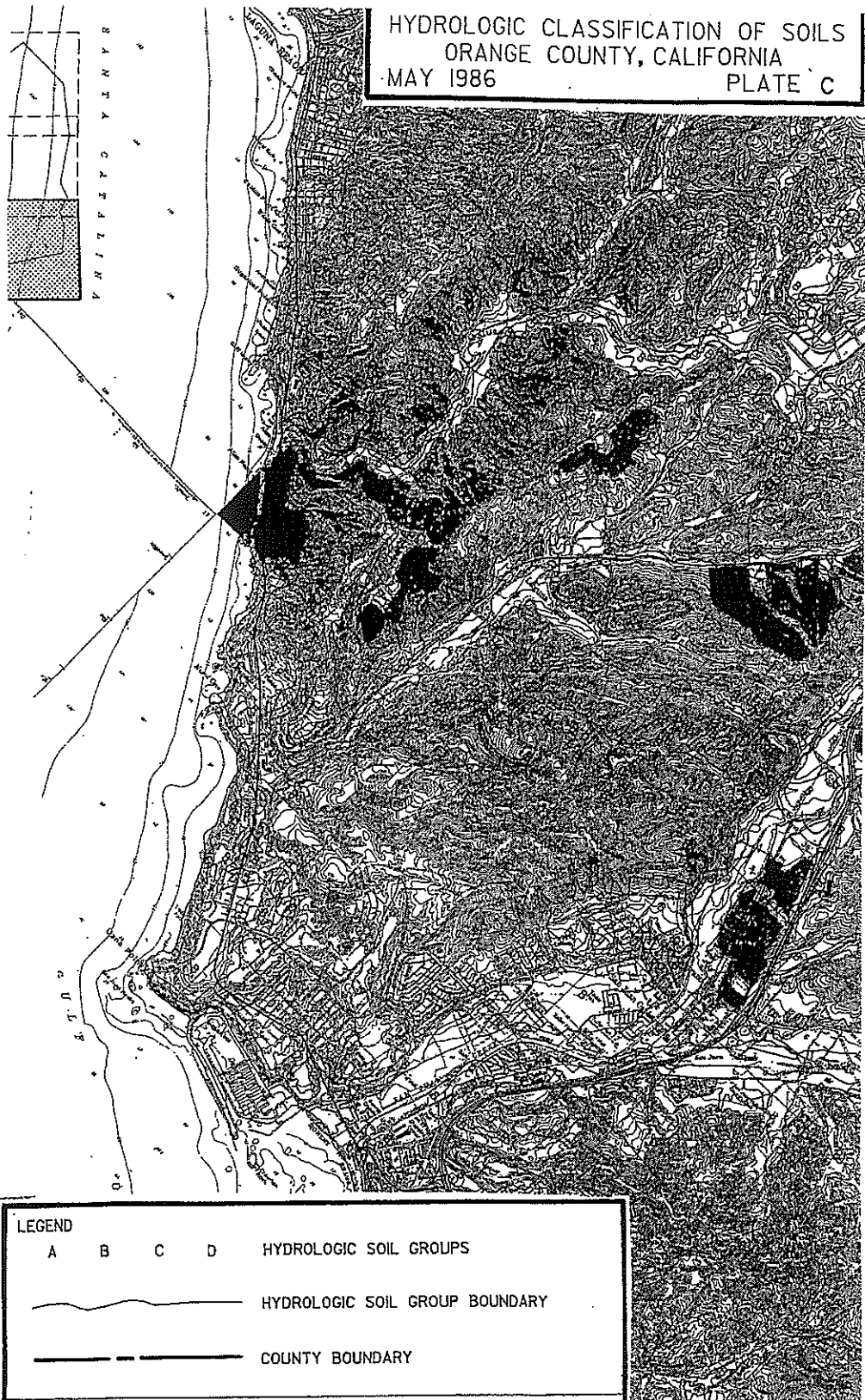
Table A-1 above shows the 25-year and 100-year storm event peak flows for the existing and post development conditions. As indicated, the proposed post development peak discharge along the northerly and easterly slopes are less than the existing condition rates. Also, the proposed post development peak discharge at the south-east corner is less than the existing condition rates as calculated by the church's original hydrology report prepared by Boyle Engineering.

## VI. VICINITY MAP

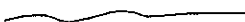

## VII. SOIL GROUP MAP



HYDROLOGIC CLASSIFICATION OF SOILS  
ORANGE COUNTY, CALIFORNIA  
MAY 1986  
PLATE C



LEGEND

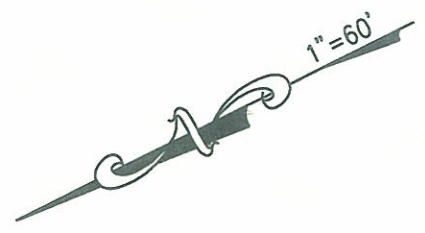
- |   |   |   |   |                                |
|---|---|---|---|--------------------------------|
| A   | B | C | D | HYDROLOGIC SOIL GROUPS         |
|  |   |   |   | HYDROLOGIC SOIL GROUP BOUNDARY |
|  |   |   |   | COUNTY BOUNDARY                |

## **VIII. DRAINAGE AREA EXHIBITS**

- **Existing Condition**
- **Developed Condition**



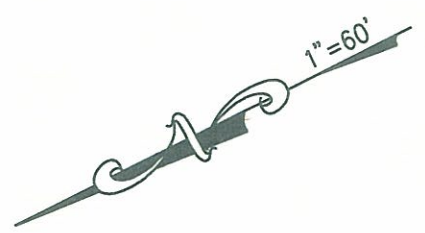
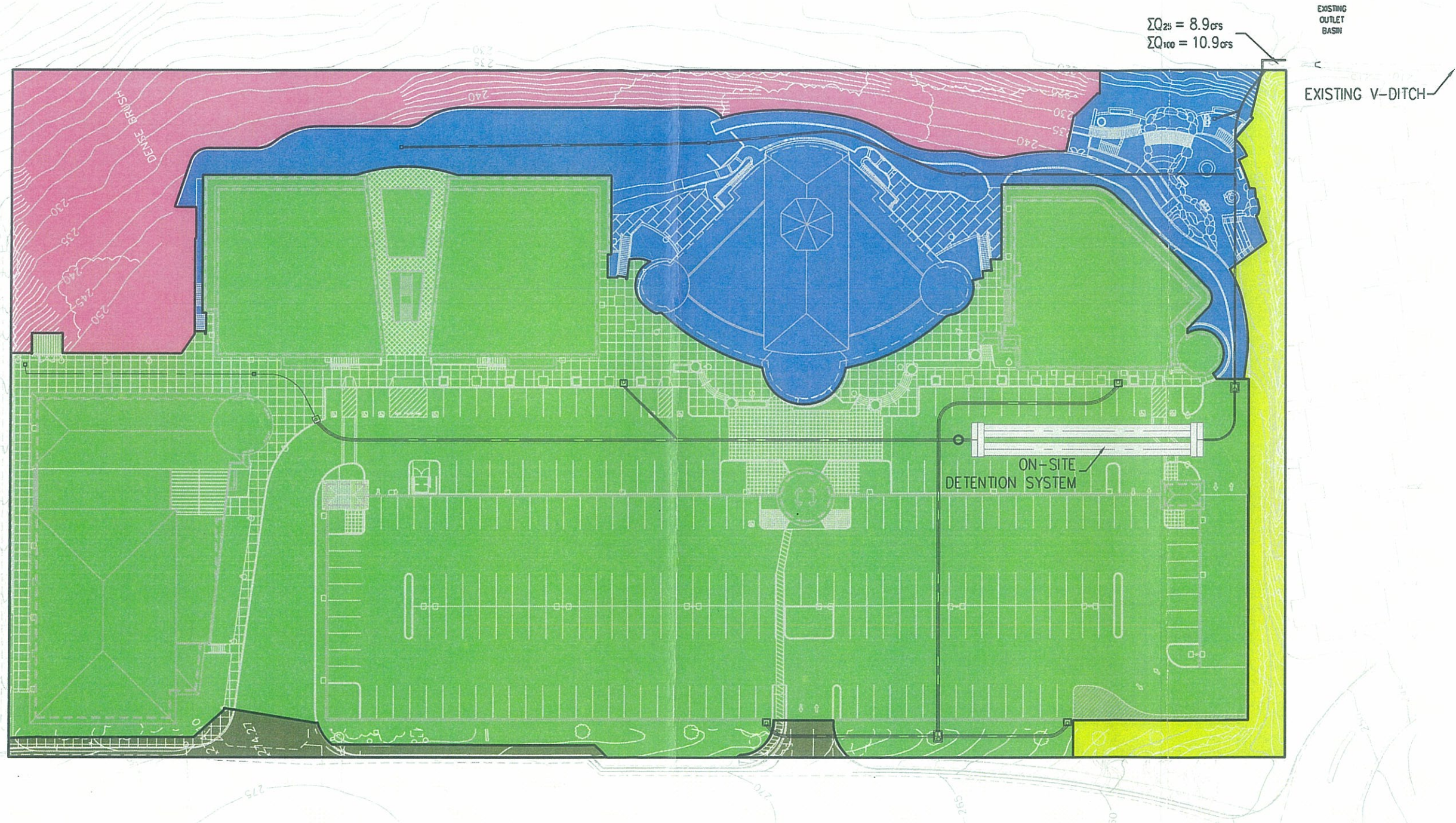
$\Sigma Q_{25} = 13.1 \text{ cfs}$   
 $\Sigma Q_{100} = 16.8 \text{ cfs}$



## DRAINAGE AREA EXHIBIT

### EXISTING CONDITION

AREA	ACREAGE	Q <sub>25</sub>	ΣQ <sub>25</sub>	Q <sub>100</sub>	ΣQ <sub>100</sub>
<span style="color: green;">■</span> AREA "A"	2.1 ACRES	9.2 CFS	13.1 CFS	11.8 CFS	16.8 CFS
<span style="color: blue;">■</span> AREA "B"	0.8 ACRES	2.9 CFS		3.8 CFS	
<span style="color: yellow;">■</span> AREA "C"	0.3 ACRES	1.2 CFS	1.6 CFS		
<span style="color: pink;">■</span> AREA "D"	2.4 ACRES	11.3 CFS	11.3 CFS	14.3 CFS	14.3 CFS
<span style="color: darkgreen;">■</span> AREA "E"	0.4 ACRES	1.7 CFS	1.7 CFS	2.1 CFS	2.1 CFS
TOTAL	6.0 ACRES				



## DRAINAGE AREA EXHIBIT

DEVELOPED CONDITION

AREA	ACREAGE	Q <sub>25</sub>	ΣQ <sub>25</sub>	Q <sub>100</sub>	ΣQ <sub>100</sub>
<span style="color: green;">■</span> AREA "A"	4.0 ACRES	5.8* CFS	8.9 CFS	6.8* CFS	10.9 CFS
<span style="color: blue;">■</span> AREA "B"	1.0 ACRES	2.9 CFS		3.7 CFS	
<span style="color: yellow;">■</span> AREA "C"	0.2 ACRES	0.7 CFS		1.0 CFS	
<span style="color: pink;">■</span> AREA "D"	0.7 ACRES	2.8 CFS	2.8 CFS	3.6 CFS	3.6 CFS
<span style="color: brown;">■</span> AREA "E"	0.1 ACRES	0.4 CFS	0.4 CFS	0.6 CFS	0.6 CFS
<b>TOTAL</b>	<b>6.0 ACRES</b>				

\*INCLUDES FLOW REDUCTION DUE TO ON-SITE DETENTION SYSTEM

## **IX. 25-YEAR HYDROLOGY CALCULATIONS**

- **Existing 25-Year**
- **Developed 25-Year**

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
(c) Copyright 1983-2002 Advanced Engineering Software (aes)  
Ver. 8.0 Release Date: 01/01/2002 License ID 1204

Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* Q25 STORM EVENT \*  
\* SOUTH SHORES CHURCH \*  
\* EXISTING CONDITIONS \*  
\*\*\*\*\*

FILE NAME: CHURCHEX.DAT  
TIME/DATE OF STUDY: 16:57 08/10/2007

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT (YEAR) = 25.00  
SPECIFIED MINIMUM PIPE SIZE (INCH) = 6.00  
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- CROWN TO		STREET-CROSSFALL:		CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
	WIDTH (FT)	CROSSFALL (FT)	IN- SIDE	OUT- / SIDE/ WAY		WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018	0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
  2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)
- \*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 78.00  
ELEVATION DATA: UPSTREAM (FEET) = 274.60 DOWNSTREAM (FEET) = 274.20

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$  (MIN.) = 6.757  
\* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 4.068

SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
SCHOOL	D	0.20	0.20	0.60	75	6.76

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.60  
SUBAREA RUNOFF (CFS) = 0.71  
TOTAL AREA (ACRES) = 0.20 PEAK FLOW RATE (CFS) = 0.71

\*\*\*\*\*  
FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 41  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM (FEET) = 272.20 DOWNSTREAM (FEET) = 264.50  
FLOW LENGTH (FEET) = 126.00 MANNING'S N = 0.013  
ASSUME FULL-FLOWING PIPELINE  
PIPE-FLOW VELOCITY (FEET/SEC.) = 5.83  
(Pipe flow velocity corresponding to normal-depth flow  
at depth = 0.82 \* diameter)  
GIVEN PIPE DIAMETER (INCH) = 4.00 NUMBER OF PIPES = 1  
PIPE-FLOW (CFS) = 0.71  
PIPE TRAVEL TIME (MIN.) = 0.36 Tc (MIN.) = 7.12  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 204.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 102.00 TO NODE 102.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
=====

MAINLINE Tc (MIN) = 7.12  
\* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.982  
SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	0.27	0.20	0.50	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.50  
SUBAREA AREA (ACRES) = 0.27 SUBAREA RUNOFF (CFS) = 0.94  
EFFECTIVE AREA (ACRES) = 0.47 AREA-AVERAGED Fm (INCH/HR) = 0.11  
AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.54  
TOTAL AREA (ACRES) = 0.47 PEAK FLOW RATE (CFS) = 1.64

\*\*\*\*\*  
FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM (FEET) = 264.50 DOWNSTREAM (FEET) = 237.00  
CHANNEL LENGTH THRU SUBAREA (FEET) = 115.80 CHANNEL SLOPE = 0.2375  
CHANNEL BASE (FEET) = 0.00 "Z" FACTOR = 1.000  
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH (FEET) = 1.50  
\* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.922  
SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					

" .4 DWELLING/ACRE"            D            0.12            0.20            0.90            75  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.84  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 12.84  
 AVERAGE FLOW DEPTH(FEET) = 0.38    TRAVEL TIME(MIN.) = 0.15  
 Tc(MIN.) = 7.27  
 SUBAREA AREA(ACRES) = 0.12            SUBAREA RUNOFF(CFS) = 0.40  
 EFFECTIVE AREA(ACRES) = 0.59            AREA-AVERAGED Fm(INCH/HR) = 0.12  
 AREA-AVERAGED Fp(INCH/HR) = 0.20            AREA-AVERAGED Ap = 0.62  
 TOTAL AREA(ACRES) = 0.59            PEAK FLOW RATE(CFS) = 2.02

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.39    FLOW VELOCITY(FEET/SEC.) = 13.00  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 319.80 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 237.00    DOWNSTREAM(FEET) = 227.50  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 34.00    CHANNEL SLOPE = 0.2794  
 CHANNEL BASE(FEET) = 0.00    "Z" FACTOR = 1.000  
 MANNING'S FACTOR = 0.015    MAXIMUM DEPTH(FEET) = 1.50  
 CHANNEL FLOW THRU SUBAREA(CFS) = 2.02  
 FLOW VELOCITY(FEET/SEC.) = 13.66    FLOW DEPTH(FEET) = 0.38  
 TRAVEL TIME(MIN.) = 0.04    Tc(MIN.) = 7.31  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 353.80 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 104.00 TO NODE 104.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 110.00 TO NODE 111.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 31.50  
 ELEVATION DATA: UPSTREAM(FEET) = 265.30    DOWNSTREAM(FEET) = 265.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
APARTMENTS	D	0.07	0.20	0.20	75	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.20  
 SUBAREA RUNOFF(CFS) = 0.30  
 TOTAL AREA(ACRES) = 0.07    PEAK FLOW RATE(CFS) = 0.30

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 41



-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 263.00 DOWNSTREAM(FEET) = 262.50  
FLOW LENGTH(FEET) = 24.90 MANNING'S N = 0.013  
ASSUME FULL-FLOWING PIPELINE  
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.34  
(PIPE FLOW VELOCITY CORRESPONDING TO NORMAL-DEPTH FLOW  
AT DEPTH = 0.82 \* DIAMETER)  
GIVEN PIPE DIAMETER(INCH) = 4.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 0.30  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 5.12  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 112.00 = 56.40 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 112.00 TO NODE 104.00 IS CODE = 82  
-----

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<  
>>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<  
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 102.10  
ELEVATION DATA: UPSTREAM(FEET) = 262.50 DOWNSTREAM(FEET) = 227.50

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
-------------------------------	-------------------	-----------------	-----------------	-----------------	-----------	--------------

RESIDENTIAL ".4 DWELLING/ACRE"	D	0.11	0.20	0.90	75	5.00
-----------------------------------	---	------	------	------	----	------

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90

SUBAREA AREA(ACRES) = 0.11 INITIAL SUBAREA RUNOFF(CFS) = 0.46

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:

MAINLINE Tc(MIN) = 5.12

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.771

SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.45

EFFECTIVE AREA(ACRES) = 0.18 AREA-AVERAGED Fm(INCH/HR) = 0.13

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.63

TOTAL AREA(ACRES) = 0.18 PEAK FLOW RATE(CFS) = 0.75

\*\*\*\*\*  
FLOW PROCESS FROM NODE 104.00 TO NODE 104.00 IS CODE = 11  
-----

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<  
=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	0.75	5.12	4.771	0.20( 0.13)	0.63	0.2	110.00

LONGEST FLOWPATH FROM NODE 110.00 TO NODE 104.00 = 56.40 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.02	7.31	3.906	0.20( 0.12)	0.62	0.6	100.00

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 353.80 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.49	5.12	4.771	0.20( 0.12)	0.62	0.6	110.00
2	2.63	7.31	3.906	0.20( 0.12)	0.62	0.8	100.00
TOTAL AREA(ACRES) =			0.77				

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.63 Tc(MIN.) = 7.309  
EFFECTIVE AREA(ACRES) = 0.77 AREA-AVERAGED Fm(INCH/HR) = 0.12  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.62  
TOTAL AREA(ACRES) = 0.77  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 353.80 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 120.00 TO NODE 121.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 33.70  
ELEVATION DATA: UPSTREAM(FEET) = 265.30 DOWNSTREAM(FEET) = 264.60

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820  
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
APARTMENTS	D	0.06	0.20	0.20	75	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.20  
SUBAREA RUNOFF(CFS) = 0.26  
TOTAL AREA(ACRES) = 0.06 PEAK FLOW RATE(CFS) = 0.26

\*\*\*\*\*

FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 82

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<  
>>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 171.20  
ELEVATION DATA: UPSTREAM(FEET) = 264.60 DOWNSTREAM(FEET) = 190.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820  
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL ".4 DWELLING/ACRE"	D	0.39	0.20	0.90	75	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90  
SUBAREA AREA(ACRES) = 0.39 INITIAL SUBAREA RUNOFF(CFS) = 1.63

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:  
MAINLINE Tc(MIN) = 5.00

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820  
 SUBAREA AREA(ACRES) = 0.39 SUBAREA RUNOFF(CFS) = 1.63  
 EFFECTIVE AREA(ACRES) = 0.45 AREA-AVERAGED Fm(INCH/HR) = 0.16  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.81  
 TOTAL AREA(ACRES) = 0.45 PEAK FLOW RATE(CFS) = 1.89

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 130.00 TO NODE 131.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 68.00  
 ELEVATION DATA: UPSTREAM(FEET) = 274.30 DOWNSTREAM(FEET) = 264.50

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "8-10 DWELLINGS/ACRE"	D	0.09	0.20	0.40	75	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.40  
 SUBAREA RUNOFF(CFS) = 0.38  
 TOTAL AREA(ACRES) = 0.09 PEAK FLOW RATE(CFS) = 0.38

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 131.00 TO NODE 132.00 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 262.50 DOWNSTREAM(FEET) = 254.50  
 FLOW LENGTH(FEET) = 58.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 6.0 INCH PIPE IS 1.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.76  
 GIVEN PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.38  
 PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 5.12  
 LONGEST FLOWPATH FROM NODE 130.00 TO NODE 132.00 = 126.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 132.00 TO NODE 132.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN) = 5.12  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.771  
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL ".4 DWELLING/ACRE"	D	0.09	0.20	0.90	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90  
 SUBAREA AREA(ACRES) = 0.09 SUBAREA RUNOFF(CFS) = 0.37  
 EFFECTIVE AREA(ACRES) = 0.18 AREA-AVERAGED Fm(INCH/HR) = 0.13  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.65

TOTAL AREA(ACRES) = 0.18 PEAK FLOW RATE(CFS) = 0.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 132.00 TO NODE 133.00 IS CODE = 82

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<<  
>>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 97.00  
ELEVATION DATA: UPSTREAM(FEET) = 254.50 DOWNSTREAM(FEET) = 225.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
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RESIDENTIAL

" .4 DWELLING/ACRE" D 0.18 0.20 0.90 75 5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90

SUBAREA AREA(ACRES) = 0.18 INITIAL SUBAREA RUNOFF(CFS) = 0.75

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:

MAINLINE Tc(MIN) = 5.12

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.771

SUBAREA AREA(ACRES) = 0.18 SUBAREA RUNOFF(CFS) = 0.74

EFFECTIVE AREA(ACRES) = 0.36 AREA-AVERAGED Fm(INCH/HR) = 0.16

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.78

TOTAL AREA(ACRES) = 0.36 PEAK FLOW RATE(CFS) = 1.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 140.00 TO NODE 141.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 67.00  
ELEVATION DATA: UPSTREAM(FEET) = 265.50 DOWNSTREAM(FEET) = 264.70

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.070

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.792

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
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RESIDENTIAL

"5-7 DWELLINGS/ACRE" D 0.09 0.20 0.50 75 5.07

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.50

SUBAREA RUNOFF(CFS) = 0.38

TOTAL AREA(ACRES) = 0.09 PEAK FLOW RATE(CFS) = 0.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 141.00 TO NODE 142.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 262.70 DOWNSTREAM(FEET) = 254.50

FLOW LENGTH(FEET) = 88.50 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 6.0 INCH PIPE IS 2.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.77  
 GIVEN PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.38  
 PIPE TRAVEL TIME(MIN.) = 0.22 Tc(MIN.) = 5.29  
 LONGEST FLOWPATH FROM NODE 140.00 TO NODE 142.00 = 155.50 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 142.00 TO NODE 143.00 IS CODE = 82

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<  
 >>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 88.50  
 ELEVATION DATA: UPSTREAM(FEET) = 254.50 DOWNSTREAM(FEET) = 235.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL ".4 DWELLING/ACRE"	D	0.17	0.20	0.90	75	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90

SUBAREA AREA(ACRES) = 0.17 INITIAL SUBAREA RUNOFF(CFS) = 0.71

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:

MAINLINE Tc(MIN) = 5.29

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.706

SUBAREA AREA(ACRES) = 0.17 SUBAREA RUNOFF(CFS) = 0.69

EFFECTIVE AREA(ACRES) = 0.26 AREA-AVERAGED Fm(INCH/HR) = 0.15

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.76

TOTAL AREA(ACRES) = 0.26 PEAK FLOW RATE(CFS) = 1.07

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 132.00  
 ELEVATION DATA: UPSTREAM(FEET) = 265.00 DOWNSTREAM(FEET) = 235.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL ".4 DWELLING/ACRE"	D	0.21	0.20	0.90	75	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90

SUBAREA RUNOFF(CFS) = 0.88

TOTAL AREA(ACRES) = 0.21 PEAK FLOW RATE(CFS) = 0.88

\*\*\*\*\*

FLOW PROCESS FROM NODE 210.00 TO NODE 211.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 87.50  
ELEVATION DATA: UPSTREAM(FEET) = 251.00 DOWNSTREAM(FEET) = 216.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
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RESIDENTIAL

".4 DWELLING/ACRE" D 0.32 0.20 0.90 75 5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.90

SUBAREA RUNOFF(CFS) = 1.34

TOTAL AREA(ACRES) = 0.32 PEAK FLOW RATE(CFS) = 1.34

\*\*\*\*\*  
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 172.00  
ELEVATION DATA: UPSTREAM(FEET) = 265.80 DOWNSTREAM(FEET) = 251.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
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CONDOMINIUMS

D 0.19 0.20 0.35 75 5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.35

SUBAREA RUNOFF(CFS) = 0.81

TOTAL AREA(ACRES) = 0.19 PEAK FLOW RATE(CFS) = 0.81

\*\*\*\*\*  
FLOW PROCESS FROM NODE 301.00 TO NODE 301.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE  $T_c$ (MIN) = 5.00  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
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COMMERCIAL D 0.11 0.20 0.10 75

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.10

SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.48

EFFECTIVE AREA(ACRES) = 0.30 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.05

AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.26

TOTAL AREA(ACRES) = 0.30 PEAK FLOW RATE(CFS) = 1.29

\*\*\*\*\*

FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 249.00 DOWNSTREAM(FEET) = 247.00  
FLOW LENGTH(FEET) = 101.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.14  
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.29  
PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 5.33  
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 273.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 302.00 TO NODE 302.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN) = 5.33  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.690  
SUBAREA LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
COMMERCIAL D 0.12 0.20 0.10 75  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.10  
SUBAREA AREA(ACRES) = 0.12 SUBAREA RUNOFF(CFS) = 0.50  
EFFECTIVE AREA(ACRES) = 0.42 AREA-AVERAGED Fm(INCH/HR) = 0.04  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.21  
TOTAL AREA(ACRES) = 0.42 PEAK FLOW RATE(CFS) = 1.76

\*\*\*\*\*

FLOW PROCESS FROM NODE 302.00 TO NODE 303.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 247.00 DOWNSTREAM(FEET) = 245.00  
FLOW LENGTH(FEET) = 101.50 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 5.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.59  
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 1.76  
PIPE TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 5.63  
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 303.00 = 374.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 303.00 TO NODE 303.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 310.00 TO NODE 311.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

\*\*\*\*\*

INITIAL SUBAREA FLOW-LENGTH(FEET) = 141.00  
 ELEVATION DATA: UPSTREAM(FEET) = 252.50 DOWNSTREAM(FEET) = 249.80

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 7.489

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.834

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
RESIDENTIAL						
"1 DWELLING/ACRE"	D	0.23	0.20	0.80	75	7.49

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.80  
 SUBAREA RUNOFF(CFS) = 0.76  
 TOTAL AREA(ACRES) = 0.23 PEAK FLOW RATE(CFS) = 0.76

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 311.00 TO NODE 311.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE  $T_c$ (MIN) = 7.49

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.834

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
COMMERCIAL	D	0.11	0.20	0.10	75

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.10  
 SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.38  
 EFFECTIVE AREA(ACRES) = 0.34 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.11  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.57  
 TOTAL AREA(ACRES) = 0.34 PEAK FLOW RATE(CFS) = 1.14

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 311.00 TO NODE 303.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 247.80 DOWNSTREAM(FEET) = 245.00  
 FLOW LENGTH(FEET) = 26.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 8.0 INCH PIPE IS 3.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 9.45  
 GIVEN PIPE DIAMETER(INCH) = 8.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.14  
 PIPE TRAVEL TIME(MIN.) = 0.05  $T_c$ (MIN.) = 7.53  
 LONGEST FLOWPATH FROM NODE 310.00 TO NODE 303.00 = 167.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 303.00 TO NODE 303.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	$T_c$ (MIN.)	Intensity (INCH/HR)	$F_p$ ( $F_m$ ) (INCH/HR)	$A_p$ (ACRES)	$A_e$ (ACRES)	HEADWATER NODE
1	1.14	7.53	3.822	0.20(0.11)	0.57	0.3	310.00

LONGEST FLOWPATH FROM NODE 310.00 TO NODE 303.00 = 167.00 FEET.



\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	1.76	5.63	4.570	0.20 ( 0.04)	0.21	0.4	300.00

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 303.00 = 374.50 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.78	5.63	4.570	0.20 ( 0.07)	0.35	0.7	300.00
2	2.60	7.53	3.822	0.20 ( 0.07)	0.37	0.8	310.00
TOTAL AREA (ACRES) =		0.76					

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 2.78 Tc (MIN.) = 5.630  
 EFFECTIVE AREA (ACRES) = 0.67 AREA-AVERAGED Fm (INCH/HR) = 0.07  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.37  
 TOTAL AREA (ACRES) = 0.76  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 303.00 = 374.50 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 303.00 TO NODE 403.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 245.00 DOWNSTREAM (FEET) = 225.70  
 FLOW LENGTH (FEET) = 81.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.3 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 15.62  
 GIVEN PIPE DIAMETER (INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 2.78  
 PIPE TRAVEL TIME (MIN.) = 0.09 Tc (MIN.) = 5.72  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 403.00 = 455.50 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN) = 5.72  
 \* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 4.536  
 SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL ".4 DWELLING/ACRE"	D	0.05	0.20	0.90	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90  
 SUBAREA AREA (ACRES) = 0.05 SUBAREA RUNOFF (CFS) = 0.20  
 EFFECTIVE AREA (ACRES) = 0.72 AREA-AVERAGED Fm (INCH/HR) = 0.08  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.39  
 TOTAL AREA (ACRES) = 0.81 PEAK FLOW RATE (CFS) = 2.91

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 400.00 TO NODE 401.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 62.00
ELEVATION DATA: UPSTREAM(FEET) = 275.20 DOWNSTREAM(FEET) = 273.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL D 0.10 0.20 0.10 75 5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.10

SUBAREA RUNOFF(CFS) = 0.43

TOTAL AREA(ACRES) = 0.10 PEAK FLOW RATE(CFS) = 0.43

\*\*\*\*\*

FLOW PROCESS FROM NODE 401.00 TO NODE 402.00 IS CODE = 82

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<
>>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 509.00
ELEVATION DATA: UPSTREAM(FEET) = 273.00 DOWNSTREAM(FEET) = 250.50

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.862

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.083

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL D 2.03 0.20 0.10 75 6.86

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.10

SUBAREA AREA(ACRES) = 2.03 INITIAL SUBAREA RUNOFF(CFS) = 7.42

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:

MAINLINE Tc(MIN) = 5.00

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820

SUBAREA AREA(ACRES) = 2.03 SUBAREA RUNOFF(CFS) = 8.77

EFFECTIVE AREA(ACRES) = 2.13 AREA-AVERAGED Fm(INCH/HR) = 0.02

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10

TOTAL AREA(ACRES) = 2.13 PEAK FLOW RATE(CFS) = 9.20

\*\*\*\*\*

FLOW PROCESS FROM NODE 402.00 TO NODE 403.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 243.60 DOWNSTREAM(FEET) = 225.70
FLOW LENGTH(FEET) = 123.30 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.82

GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.20  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 5.12  
LONGEST FLOWPATH FROM NODE 400.00 TO NODE 403.00 = 185.30 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<  
=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	9.20	5.12	4.774	0.20( 0.02)	0.10	2.1	400.00

LONGEST FLOWPATH FROM NODE 400.00 TO NODE 403.00 = 185.30 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.91	5.72	4.536	0.20( 0.08)	0.39	0.7	300.00
2	2.71	7.62	3.802	0.20( 0.08)	0.41	0.8	310.00

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 403.00 = 455.50 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.94	5.12	4.774	0.20( 0.03)	0.17	2.8	400.00
2	11.65	5.72	4.536	0.20( 0.03)	0.17	2.9	300.00
3	10.03	7.62	3.802	0.20( 0.04)	0.18	2.9	310.00

TOTAL AREA(ACRES) = 2.94

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.94 Tc(MIN.) = 5.115  
EFFECTIVE AREA(ACRES) = 2.78 AREA-AVERAGED Fm(INCH/HR) = 0.03  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.17  
TOTAL AREA(ACRES) = 2.94  
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 403.00 = 455.50 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 403.00 TO NODE 404.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 225.70 DOWNSTREAM(FEET) = 209.30  
FLOW LENGTH(FEET) = 79.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.66  
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.94  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 5.18  
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 404.00 = 534.50 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 404.00 TO NODE 502.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 211.00 DOWNSTREAM(FEET) = 210.50  
 FLOW LENGTH(FEET) = 10.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.96  
 (PIPE FLOW VELOCITY CORRESPONDING TO NORMAL-DEPTH FLOW  
 AT DEPTH = 0.82 \* DIAMETER)  
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 11.94  
 PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 5.19  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 502.00 = 544.50 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 0.00 TO NODE 0.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 502.00 TO NODE 502.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 143.00  
 ELEVATION DATA: UPSTREAM(FEET) = 263.50 DOWNSTREAM(FEET) = 252.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.869  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.476  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL ".4 DWELLING/ACRE"	D	0.07	0.20	0.90	75	5.87

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90  
 SUBAREA RUNOFF(CFS) = 0.27  
 TOTAL AREA(ACRES) = 0.07 PEAK FLOW RATE(CFS) = 0.27

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 82

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<  
 >>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 336.00  
 ELEVATION DATA: UPSTREAM(FEET) = 252.00 DOWNSTREAM(FEET) = 210.50

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.581  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.812  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
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RESIDENTIAL

".4 DWELLING/ACRE" D 0.24 0.20 0.90 75 7.58
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90
SUBAREA AREA (ACRES) = 0.24 INITIAL SUBAREA RUNOFF(CFS) = 0.78

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:

MAINLINE Tc(MIN) = 5.87

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.476

SUBAREA AREA(ACRES) = 0.24 SUBAREA RUNOFF(CFS) = 0.93

EFFECTIVE AREA(ACRES) = 0.31 AREA-AVERAGED Fm(INCH/HR) = 0.18

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.90

TOTAL AREA(ACRES) = 0.31 PEAK FLOW RATE(CFS) = 1.20

\*\*\*\*\*

FLOW PROCESS FROM NODE 502.00 TO NODE 502.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 1.20 5.87 4.476 0.20( 0.18) 0.90 0.3 500.00
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 502.00 = 143.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 11.94 5.19 4.744 0.20( 0.03) 0.17 2.8 400.00
2 11.65 5.79 4.506 0.20( 0.03) 0.17 2.9 300.00
3 10.03 7.70 3.784 0.20( 0.04) 0.18 2.9 310.00
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 502.00 = 544.50 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 13.07 5.19 4.744 0.20( 0.05) 0.23 3.1 400.00
2 12.84 5.79 4.506 0.20( 0.05) 0.24 3.2 300.00
3 12.78 5.87 4.476 0.20( 0.05) 0.24 3.2 500.00
4 11.04 7.70 3.784 0.20( 0.05) 0.25 3.2 310.00
TOTAL AREA(ACRES) = 3.25

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 13.07 Tc(MIN.) = 5.191
EFFECTIVE AREA(ACRES) = 3.05 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.24
TOTAL AREA(ACRES) = 3.25
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 502.00 = 544.50 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 3.25 TC(MIN.) = 5.19
EFFECTIVE AREA(ACRES) = 3.05 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.23
PEAK FLOW RATE(CFS) = 13.07

\*\* PEAK FLOW RATE TABLE \*\*

STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 13.07 5.19 4.744 0.20( 0.05) 0.23 3.1 400.00

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
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Analysis prepared by:

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949-474-2330

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* 25-YEAR FREQUENCY \*  
\* AREAS A, B, AND C \*  
\* SOUTH SHORES CHURCH, DANA POINT \*  
\*\*\*\*\*

FILE NAME: SSC-A-B.DAT  
TIME/DATE OF STUDY: 10:18 02/13/2012

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT (YEAR) = 25.00  
SPECIFIED MINIMUM PIPE SIZE (INCH) = 12.00  
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- CROWN TO	STREET-CROSSFALL:	CURB	GUTTER-GEOMETRIES:	MANNING	
	WIDTH CROSSFALL	IN- / OUT- / PARK-	HEIGHT	WIDTH LIP	HIKE	FACTOR
	(FT)	(FT)	(FT)	(FT)	(FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313 0.167 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:  
1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)  
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)  
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

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+-----+
| AREA - A |
|         |
|         |
+-----+

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 240.00  
ELEVATION DATA: UPSTREAM(FEET) = 274.00 DOWNSTREAM(FEET) = 265.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.250

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.692

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
COMMERCIAL	D	0.06	0.20	0.100	75	5.25

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100  
SUBAREA RUNOFF(CFS) = 0.25  
TOTAL AREA(ACRES) = 0.06 PEAK FLOW RATE(CFS) = 0.25

\*\*\*\*\*

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 41

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 263.00 DOWNSTREAM(FEET) = 261.00  
FLOW LENGTH(FEET) = 127.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.03  
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 0.25  
PIPE TRAVEL TIME(MIN.) = 0.70  $T_c$ (MIN.) = 5.95  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 367.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 102.00 TO NODE 102.00 IS CODE = 81

-----  
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE  $T_c$ (MIN.) = 5.95  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.372  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
COMMERCIAL	D	0.44	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100  
SUBAREA AREA(ACRES) = 0.44 SUBAREA RUNOFF(CFS) = 1.72  
EFFECTIVE AREA(ACRES) = 0.50 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.02  
AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.10  
TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 1.96

\*\*\*\*\*

FLOW PROCESS FROM NODE 102.00 TO NODE 102.00 IS CODE = 81

-----  
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE  $T_c$ (MIN.) = 5.95  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.372  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
COMMERCIAL	D	0.12	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA (ACRES) = 0.12 SUBAREA RUNOFF (CFS) = 0.47  
 EFFECTIVE AREA (ACRES) = 0.62 AREA-AVERAGED Fm (INCH/HR) = 0.02  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA (ACRES) = 0.6 PEAK FLOW RATE (CFS) = 2.43

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 261.00 DOWNSTREAM (FEET) = 259.50  
 FLOW LENGTH (FEET) = 45.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 5.1 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 7.54  
 GIVEN PIPE DIAMETER (INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 2.43  
 PIPE TRAVEL TIME (MIN.) = 0.10 Tc (MIN.) = 6.05  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 412.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 6.05  
 \* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 4.331  
 SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.05	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA (ACRES) = 0.05 SUBAREA RUNOFF (CFS) = 0.19  
 EFFECTIVE AREA (ACRES) = 0.67 AREA-AVERAGED Fm (INCH/HR) = 0.02  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA (ACRES) = 0.7 PEAK FLOW RATE (CFS) = 2.60

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 82  
 -----

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<  
 >>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 166.00  
 ELEVATION DATA: UPSTREAM (FEET) = 275.50 DOWNSTREAM (FEET) = 265.50

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)] \*\* 0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 5.000  
 \* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 4.824  
 SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	D	0.16	0.20	0.100	75	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA (ACRES) = 0.16 INITIAL SUBAREA RUNOFF (CFS) = 0.69

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:



MAINLINE Tc(MIN.) = 6.05  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.331  
 SUBAREA AREA(ACRES) = 0.16 SUBAREA RUNOFF(CFS) = 0.62  
 EFFECTIVE AREA(ACRES) = 0.83 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 3.22

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 259.50 DOWNSTREAM(FEET) = 259.00  
 FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.06  
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 3.22  
 PIPE TRAVEL TIME(MIN.) = 1.09 Tc(MIN.) = 7.14  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 612.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 104.00 TO NODE 104.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====  
 MAINLINE Tc(MIN.) = 7.14  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.943  
 SUBAREA LOSS RATE DATA(AMC II):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.26	0.20	0.100	75
COMMERCIAL	D	0.25	0.20	0.100	75
COMMERCIAL	D	0.41	0.20	0.100	75

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 0.92 SUBAREA RUNOFF(CFS) = 3.25  
 EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 6.18

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 259.00 DOWNSTREAM(FEET) = 248.50  
 FLOW LENGTH(FEET) = 143.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 12.64  
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 6.18  
 PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 7.33  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 105.00 = 755.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 10  
 -----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 247.00  
ELEVATION DATA: UPSTREAM(FEET) = 277.50 DOWNSTREAM(FEET) = 269.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.403

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.617

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
COMMERCIAL	D	0.50	0.20	0.100	75	5.40

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100

SUBAREA RUNOFF(CFS) = 2.07

TOTAL AREA(ACRES) = 0.50 PEAK FLOW RATE(CFS) = 2.07

\*\*\*\*\*  
FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 263.00 DOWNSTREAM(FEET) = 255.00  
FLOW LENGTH(FEET) = 96.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.61  
GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.07  
PIPE TRAVEL TIME(MIN.) = 0.17  $T_c$ (MIN.) = 5.57  
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 343.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 203.00 TO NODE 204.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 376.00  
ELEVATION DATA: UPSTREAM(FEET) = 277.50 DOWNSTREAM(FEET) = 264.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 6.338

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.218

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
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COMMERCIAL D 0.99 0.20 0.100 75 6.34  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 3.74  
 TOTAL AREA(ACRES) = 0.99 PEAK FLOW RATE(CFS) = 3.74

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 204.00 TO NODE 202.00 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 257.00 DOWNSTREAM(FEET) = 255.00  
 FLOW LENGTH(FEET) = 72.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.73  
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 3.74  
 PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 6.49  
 LONGEST FLOWPATH FROM NODE 203.00 TO NODE 202.00 = 448.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 11  
 -----

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	3.74	6.49	4.161	0.20( 0.02)	0.10	1.0	203.00

LONGEST FLOWPATH FROM NODE 203.00 TO NODE 202.00 = 448.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.07	5.57	4.538	0.20( 0.02)	0.10	0.5	200.00

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 343.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	5.57	5.57	4.538	0.20( 0.02)	0.10	1.3	200.00
2	5.64	6.49	4.161	0.20( 0.02)	0.10	1.5	203.00

TOTAL AREA(ACRES) = 1.5

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.64 Tc(MIN.) = 6.493  
 EFFECTIVE AREA(ACRES) = 1.49 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 1.5  
 LONGEST FLOWPATH FROM NODE 203.00 TO NODE 202.00 = 448.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 202.00 TO NODE 105.00 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 250.00 DOWNSTREAM(FEET) = 248.50

FLOW LENGTH (FEET) = 162.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.8 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 5.76  
 GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 5.64  
 PIPE TRAVEL TIME (MIN.) = 0.47 Tc (MIN.) = 6.96  
 LONGEST FLOWPATH FROM NODE 203.00 TO NODE 105.00 = 610.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 11

=====  
 >>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<  
 =====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	5.57	6.04	4.335	0.20 (0.02)	0.10	1.3	200.00
2	5.64	6.96	4.000	0.20 (0.02)	0.10	1.5	203.00

LONGEST FLOWPATH FROM NODE 203.00 TO NODE 105.00 = 610.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.18	7.33	3.885	0.20 (0.02)	0.10	1.8	100.00

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 105.00 = 755.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.25	6.04	4.335	0.20 (0.02)	0.10	2.8	200.00
2	11.68	6.96	4.000	0.20 (0.02)	0.10	3.2	203.00
3	11.65	7.33	3.885	0.20 (0.02)	0.10	3.2	100.00

TOTAL AREA (ACRES) = 3.2

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 11.68 Tc (MIN.) = 6.961  
 EFFECTIVE AREA (ACRES) = 3.15 AREA-AVERAGED Fm (INCH/HR) = 0.02  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA (ACRES) = 3.2  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 105.00 = 755.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 81

=====  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
 =====

MAINLINE Tc (MIN.) = 6.96  
 \* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 4.000  
 SUBAREA LOSS RATE DATA (AMC II):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.56	0.20	0.100	75
COMMERCIAL	D	0.23	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA (ACRES) = 0.79 SUBAREA RUNOFF (CFS) = 2.83  
 EFFECTIVE AREA (ACRES) = 3.94 AREA-AVERAGED Fm (INCH/HR) = 0.02  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA (ACRES) = 4.0 PEAK FLOW RATE (CFS) = 14.12

+-----+  
| ON-SITE DETENTION SYSTEM |  
| PEAK FLOW REDUCTION FROM Q25=14.12 CFS TO Q25=5.75 CFS |  
| MAXIMUM STORAGE VOLUME = 0.164 AC-FT |  
+-----+

\*\*\*\*\*  
FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN.) = 6.96 RAINFALL INTENSITY(INCH/HR) = 4.00

EFFECTIVE AREA(ACRES) = 1.60

TOTAL AREA(ACRES) = 4.00 PEAK FLOW RATE(CFS) = 5.75

AREA-AVERAGED Fm(INCH/HR) = 0.02 AREA-AVERAGED Fp(INCH/HR) = 0.20

AREA-AVERAGED Ap = 0.10

NOTE: EFFECTIVE AREA IS USED AS THE TOTAL CONTRIBUTING AREA FOR ALL  
CONFLUENCE ANALYSES.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 106.00 TO NODE 107.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 245.00 DOWNSTREAM(FEET) = 244.00

FLOW LENGTH(FEET) = 47.00 MANNING'S N = 0.013

ASSUME FULL-FLOWING PIPELINE

PIPE-FLOW VELOCITY(FEET/SEC.) = 7.32

PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)

GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 5.75

PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 7.07

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 107.00 = 802.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 244.00 DOWNSTREAM(FEET) = 225.00

FLOW LENGTH(FEET) = 120.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 12.0 INCH PIPE IS 5.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 16.78

GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 5.75

PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 7.19

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 108.00 = 922.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<

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+-----+
| AREA - B |
+-----+

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*****
FLOW PROCESS FROM NODE 400.00 TO NODE 401.00 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

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=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 133.00
ELEVATION DATA: UPSTREAM(FEET) = 250.00 DOWNSTREAM(FEET) = 248.70

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Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.619
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.544

```

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SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp        Ap        SCS      Tc
LAND USE              GROUP   (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
PUBLIC PARK           D        0.07    0.20     0.850    75     8.62
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA RUNOFF(CFS) = 0.21
TOTAL AREA(ACRES) = 0.07 PEAK FLOW RATE(CFS) = 0.21

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```

*****
FLOW PROCESS FROM NODE 401.00 TO NODE 402.00 IS CODE = 41

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```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 247.00 DOWNSTREAM(FEET) = 245.30
FLOW LENGTH(FEET) = 168.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.48
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.21
PIPE TRAVEL TIME(MIN.) = 1.13 Tc(MIN.) = 9.75
LONGEST FLOWPATH FROM NODE 400.00 TO NODE 402.00 = 301.00 FEET.

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*****
FLOW PROCESS FROM NODE 402.00 TO NODE 402.00 IS CODE = 82

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```

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<
>>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

```

```

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 163.00
ELEVATION DATA: UPSTREAM(FEET) = 250.00 DOWNSTREAM(FEET) = 248.40

```

```

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.969
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.705

```

```

SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp        Ap        SCS      Tc
LAND USE              GROUP   (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
SCHOOL                D        0.23    0.20     0.600    75     7.97
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.600

```

SUBAREA AREA(ACRES) = 0.23 INITIAL SUBAREA RUNOFF(CFS) = 0.74

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:

MAINLINE Tc(MIN.) = 9.75

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.305

SUBAREA AREA(ACRES) = 0.23 SUBAREA RUNOFF(CFS) = 0.66

EFFECTIVE AREA(ACRES) = 0.30 AREA-AVERAGED Fm(INCH/HR) = 0.13

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.66

TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 0.86

\*\*\*\*\*  
FLOW PROCESS FROM NODE 402.00 TO NODE 402.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 9.75

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.305

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.11	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.33

EFFECTIVE AREA(ACRES) = 0.41 AREA-AVERAGED Fm(INCH/HR) = 0.10

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.51

TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 1.18

\*\*\*\*\*  
FLOW PROCESS FROM NODE 402.00 TO NODE 403.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 245.30 DOWNSTREAM(FEET) = 243.80

FLOW LENGTH(FEET) = 144.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.8 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 4.05

GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 1.18

PIPE TRAVEL TIME(MIN.) = 0.59 Tc(MIN.) = 10.34

LONGEST FLOWPATH FROM NODE 400.00 TO NODE 403.00 = 445.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 10.34

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.197

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.12	0.20	0.100	75
COMMERCIAL	D	0.11	0.20	0.100	75
COMMERCIAL	D	0.11	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 0.34 SUBAREA RUNOFF(CFS) = 0.97

EFFECTIVE AREA(ACRES) = 0.75 AREA-AVERAGED Fm(INCH/HR) = 0.06

AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.32  
TOTAL AREA (ACRES) = 0.8 PEAK FLOW RATE (CFS) = 2.11

\*\*\*\*\*  
FLOW PROCESS FROM NODE 403.00 TO NODE 108.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 243.80 DOWNSTREAM (FEET) = 225.00  
FLOW LENGTH (FEET) = 150.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.4 INCHES  
PIPE-FLOW VELOCITY (FEET/SEC.) = 11.70  
GIVEN PIPE DIAMETER (INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW (CFS) = 2.11  
PIPE TRAVEL TIME (MIN.) = 0.21 Tc (MIN.) = 10.56  
LONGEST FLOWPATH FROM NODE 400.00 TO NODE 108.00 = 595.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.11	10.56	3.160	0.20 (0.06)	0.32	0.8	400.00

LONGEST FLOWPATH FROM NODE 400.00 TO NODE 108.00 = 595.00 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	5.75	7.19	3.928	0.20 (0.02)	0.10	1.6	100.00

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 108.00 = 922.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	7.55	7.19	3.928	0.20 (0.03)	0.15	2.1	100.00
2	6.73	10.56	3.160	0.20 (0.03)	0.17	2.3	400.00

TOTAL AREA (ACRES) = 4.8

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 7.55 Tc (MIN.) = 7.186  
EFFECTIVE AREA (ACRES) = 2.11 AREA-AVERAGED Fm (INCH/HR) = 0.03  
AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.17  
TOTAL AREA (ACRES) = 4.8  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 108.00 = 922.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 108.00 TO NODE 109.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 225.00 DOWNSTREAM (FEET) = 220.00  
FLOW LENGTH (FEET) = 35.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.5 INCHES  
PIPE-FLOW VELOCITY (FEET/SEC.) = 17.29



GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 7.55  
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 7.22  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 109.00 = 957.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 109.00 TO NODE 109.00 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 7.22  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.918  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.22	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 0.22 SUBAREA RUNOFF(CFS) = 0.77  
EFFECTIVE AREA(ACRES) = 2.33 AREA-AVERAGED Fm(INCH/HR) = 0.03  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.15  
TOTAL AREA(ACRES) = 5.0 PEAK FLOW RATE(CFS) = 8.16

\*\*\*\*\*  
FLOW PROCESS FROM NODE 109.00 TO NODE 110.00 IS CODE = 41  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 220.00 DOWNSTREAM(FEET) = 210.00  
FLOW LENGTH(FEET) = 27.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 5.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 25.18  
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.16  
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 7.24  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 110.00 = 984.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 12  
-----

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 10  
-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

-----+-----  
| AREA - C |  
| |  
| |  
+-----+-----

\*\*\*\*\*  
FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 170.00  
ELEVATION DATA: UPSTREAM(FEET) = 263.00 DOWNSTREAM(FEET) = 248.00

$$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$$

SUBAREA ANALYSIS USED MINIMUM  $T_c$  (MIN.) = 6.123

\* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 4.301

SUBAREA  $T_c$  AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
PUBLIC PARK	D	0.08	0.20	0.850	75	6.12

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$  (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.850  
SUBAREA RUNOFF (CFS) = 0.30  
TOTAL AREA (ACRES) = 0.08 PEAK FLOW RATE (CFS) = 0.30

\*\*\*\*\*  
FLOW PROCESS FROM NODE 501.00 TO NODE 110.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 248.00 DOWNSTREAM(FEET) = 210.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 292.00 CHANNEL SLOPE = 0.1301  
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 2.000  
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.50  
\* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 4.046

SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
NATURAL FAIR COVER "CHAPARRAL, BROADLEAF"	D	0.13	0.20	1.000	81

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$  (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 1.000  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 0.52  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 6.97  
AVERAGE FLOW DEPTH (FEET) = 0.19 TRAVEL TIME (MIN.) = 0.70  
 $T_c$  (MIN.) = 6.82  
SUBAREA AREA (ACRES) = 0.13 SUBAREA RUNOFF (CFS) = 0.45  
EFFECTIVE AREA (ACRES) = 0.21 AREA-AVERAGED  $F_m$  (INCH/HR) = 0.19  
AREA-AVERAGED  $F_p$  (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.94  
TOTAL AREA (ACRES) = 0.2 PEAK FLOW RATE (CFS) = 0.73

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH (FEET) = 0.22 FLOW VELOCITY (FEET/SEC.) = 7.64  
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 110.00 = 462.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	$T_c$ (MIN.)	Intensity (INCH/HR)	$F_p$ ( $F_m$ ) (INCH/HR)	$A_p$	$A_e$ (ACRES)	HEADWATER NODE
1	0.73	6.82	4.046	0.20 (0.19)	0.94	0.2	500.00

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 110.00 = 462.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	8.16	7.24	3.913	0.20( 0.03)	0.15	2.3	100.00
2	7.22	10.61	3.151	0.20( 0.03)	0.17	2.6	400.00
LONGEST FLOWPATH FROM NODE					100.00 TO NODE	110.00 =	984.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	8.68	6.82	4.046	0.20( 0.04)	0.22	2.4	500.00
2	8.86	7.24	3.913	0.20( 0.04)	0.21	2.5	100.00
3	7.78	10.61	3.151	0.20( 0.04)	0.22	2.8	400.00
TOTAL AREA(ACRES) =		5.2					

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.86 Tc(MIN.) = 7.238  
 EFFECTIVE AREA(ACRES) = 2.54 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.21  
 TOTAL AREA(ACRES) = 5.2  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 110.00 = 984.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 5.2 TC(MIN.) = 7.24  
 EFFECTIVE AREA(ACRES) = 2.54 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.215  
 PEAK FLOW RATE(CFS) = 8.86

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	8.68	6.82	4.046	0.20( 0.04)	0.22	2.4	500.00
2	8.86	7.24	3.913	0.20( 0.04)	0.21	2.5	100.00
3	7.78	10.61	3.151	0.20( 0.04)	0.22	2.8	400.00

END OF RATIONAL METHOD ANALYSIS

2	12.84	5.79	4.506	0.20( 0.05)	0.24	3.2	300.00
3	12.78	5.87	4.476	0.20( 0.05)	0.24	3.2	500.00
4	11.04	7.70	3.784	0.20( 0.05)	0.25	3.2	310.00

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END OF RATIONAL METHOD ANALYSIS

\*\*\*\*\*  
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Analysis prepared by:

Adams-Streeter Civil Engineers, Inc.  
15 Corporate Park  
Irvine, CA 92606  
949-474-2330

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* PROPOSED CONDITION - AREA "D" \*  
\* 25-YEAR FREQUENCY STORM \*  
\* SOUTH SHORES CHURCH, DANA POINT, CA \*  
\*\*\*\*\*  
FILE NAME: SSC-D-25.DAT  
TIME/DATE OF STUDY: 19:15 09/19/2011

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 25.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 12.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF-	CROWN TO	STREET-CROSSFALL:			CURB	GUTTER-GEOMETRIES:		MANNING	
	WIDTH	CROSSFALL	IN-	/	OUT-/PARK-	HEIGHT	WIDTH	LIP	HIKE	FACTOR
	(FT)	(FT)	SIDE	/	SIDE/	(FT)	(FT)	(FT)	(FT)	(n)
1	30.0	20.0	0.018/0.018/0.020			0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
  - (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)
- \*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 600.00 TO NODE 601.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 175.00  
ELEVATION DATA: UPSTREAM(FEET) = 251.00 DOWNSTREAM(FEET) = 192.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.150  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.744  
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL POOR COVER						
"CHAPARRAL, NARROWLEAF"	D	0.33	0.20	1.000	91	5.15
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20						
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000						
SUBAREA RUNOFF(CFS) = 1.35						
TOTAL AREA(ACRES) = 0.33 PEAK FLOW RATE(CFS) = 1.35						

\*\*\*\*\*  
FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 54.00  
ELEVATION DATA: UPSTREAM(FEET) = 239.00 DOWNSTREAM(FEET) = 224.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.824

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL POOR COVER						
"CHAPARRAL, NARROWLEAF"	D	0.19	0.20	1.000	91	5.00
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20						
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000						
SUBAREA RUNOFF(CFS) = 0.79						
TOTAL AREA(ACRES) = 0.19 PEAK FLOW RATE(CFS) = 0.79						

\*\*\*\*\*  
FLOW PROCESS FROM NODE 800.00 TO NODE 801.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
ELEVATION DATA: UPSTREAM(FEET) = 244.00 DOWNSTREAM(FEET) = 219.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.824

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL POOR COVER						
"CHAPARRAL, NARROWLEAF"	D	0.16	0.20	1.000	91	5.00
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20						
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000						
SUBAREA RUNOFF(CFS) = 0.67						
TOTAL AREA(ACRES) = 0.16 PEAK FLOW RATE(CFS) = 0.67						

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 0.2 TC(MIN.) = 5.00  
EFFECTIVE AREA(ACRES) = 0.16 AREA-AVERAGED Fm(INCH/HR) = 0.20  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 1.000  
PEAK FLOW RATE(CFS) = 0.67

=====

END OF RATIONAL METHOD ANALYSIS

## **X. 100-YEAR HYDROLOGY CALCULATIONS**

- **Existing 100-Year**
- **Developed 100-Year**

\*\*\*\*\*  
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Ver. 8.0 Release Date: 01/01/2002 License ID 1204

Analysis prepared by:

Adams-Streeter Civil Engineers, Inc.  
15 Corporate Park  
Irvine, CA 92606  
949-474-2330

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* Q100 STORM EVENT \*  
\* SOUTH SHORES CHURCH \*  
\* EXISTING CONDITIONS \*  
\*\*\*\*\*

FILE NAME: CHURCHEX.DAT  
TIME/DATE OF STUDY: 15:01 08/24/2007

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT (YEAR) = 100.00  
SPECIFIED MINIMUM PIPE SIZE (INCH) = 6.00  
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- CROWN TO STREET-CROSSFALL:			CURB GUTTER-GEOMETRIES:			MANNING FACTOR (n)	
	WIDTH (FT)	CROSSFALL (FT)	IN- / OUT- / SIDE / SIDE / WAY	HEIGHT (FT)	WIDTH (FT)	LIP (FT)		HIKE (FT)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:  
1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)  
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)  
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 78.00  
ELEVATION DATA: UPSTREAM (FEET) = 274.60 DOWNSTREAM (FEET) = 274.20

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 6.757  
\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 5.207



SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
SCHOOL	D	0.20	0.20	0.60	91	6.76

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.60  
 SUBAREA RUNOFF(CFS) = 0.92  
 TOTAL AREA(ACRES) = 0.20 PEAK FLOW RATE(CFS) = 0.92

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 272.20 DOWNSTREAM(FEET) = 264.50  
 FLOW LENGTH(FEET) = 126.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.83  
 (PIPE FLOW VELOCITY CORRESPONDING TO NORMAL-DEPTH FLOW  
 AT DEPTH = 0.82 \* DIAMETER)  
 GIVEN PIPE DIAMETER(INCH) = 4.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.92  
 PIPE TRAVEL TIME(MIN.) = 0.36 Tc(MIN.) = 7.12  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 204.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 102.00 TO NODE 102.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN) = 7.12  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.097  
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	0.27	0.20	0.50	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.50  
 SUBAREA AREA(ACRES) = 0.27 SUBAREA RUNOFF(CFS) = 1.21  
 EFFECTIVE AREA(ACRES) = 0.47 AREA-AVERAGED Fm(INCH/HR) = 0.11  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.54  
 TOTAL AREA(ACRES) = 0.47 PEAK FLOW RATE(CFS) = 2.11

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 264.50 DOWNSTREAM(FEET) = 237.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 115.80 CHANNEL SLOPE = 0.2375  
 CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 1.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.50  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.025  
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					

" .4 DWELLING/ACRE"                    D            0.12            0.20            0.90            91  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =            2.37  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 13.66  
 AVERAGE FLOW DEPTH(FEET) = 0.42    TRAVEL TIME(MIN.) = 0.14  
 Tc(MIN.) = 7.26  
 SUBAREA AREA(ACRES) = 0.12            SUBAREA RUNOFF(CFS) = 0.52  
 EFFECTIVE AREA(ACRES) = 0.59            AREA-AVERAGED Fm(INCH/HR) = 0.12  
 AREA-AVERAGED Fp(INCH/HR) = 0.20    AREA-AVERAGED Ap = 0.62  
 TOTAL AREA(ACRES) = 0.59            PEAK FLOW RATE(CFS) = 2.60

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.43    FLOW VELOCITY(FEET/SEC.) = 13.95  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 319.80 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 51

-----  
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 237.00    DOWNSTREAM(FEET) = 227.50  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 34.00    CHANNEL SLOPE = 0.2794  
 CHANNEL BASE(FEET) = 0.00    "Z" FACTOR = 1.000  
 MANNING'S FACTOR = 0.015    MAXIMUM DEPTH(FEET) = 1.50  
 CHANNEL FLOW THRU SUBAREA(CFS) = 2.60  
 FLOW VELOCITY(FEET/SEC.) = 14.58    FLOW DEPTH(FEET) = 0.42  
 TRAVEL TIME(MIN.) = 0.04    Tc(MIN.) = 7.30  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 353.80 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 104.00 TO NODE 104.00 IS CODE = 10

-----  
 >>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 110.00 TO NODE 111.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 31.50  
 ELEVATION DATA: UPSTREAM(FEET) = 265.30    DOWNSTREAM(FEET) = 265.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.190

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
APARTMENTS	D	0.07	0.20	0.20	91	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.20  
 SUBAREA RUNOFF(CFS) = 0.39  
 TOTAL AREA(ACRES) = 0.07    PEAK FLOW RATE(CFS) = 0.39

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 111.00 TO NODE 112.00 IS CODE = 41

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 263.00 DOWNSTREAM(FEET) = 262.50  
FLOW LENGTH(FEET) = 24.90 MANNING'S N = 0.013  
ASSUME FULL-FLOWING PIPELINE  
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.34  
(PIPE FLOW VELOCITY CORRESPONDING TO NORMAL-DEPTH FLOW  
AT DEPTH = 0.82 \* DIAMETER)  
GIVEN PIPE DIAMETER(INCH) = 4.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 0.39  
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 5.12  
LONGEST FLOWPATH FROM NODE 110.00 TO NODE 112.00 = 56.40 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 112.00 TO NODE 104.00 IS CODE = 82

-----  
>>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<  
>>>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 102.10  
ELEVATION DATA: UPSTREAM(FEET) = 262.50 DOWNSTREAM(FEET) = 227.50

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.190  
SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL ".4 DWELLING/ACRE"	D	0.11	0.20	0.90	91	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90  
SUBAREA AREA(ACRES) = 0.11 INITIAL SUBAREA RUNOFF(CFS) = 0.59

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:  
MAINLINE Tc(MIN) = 5.12  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.126  
SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.59  
EFFECTIVE AREA(ACRES) = 0.18 AREA-AVERAGED Fm(INCH/HR) = 0.13  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.63  
TOTAL AREA(ACRES) = 0.18 PEAK FLOW RATE(CFS) = 0.97

\*\*\*\*\*  
FLOW PROCESS FROM NODE 104.00 TO NODE 104.00 IS CODE = 11

-----  
>>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap (ACRES)	Ae (ACRES)	HEADWATER NODE
1	0.97	5.12	6.126	0.20( 0.13)	0.63	0.2	110.00

LONGEST FLOWPATH FROM NODE 110.00 TO NODE 104.00 = 56.40 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap (ACRES)	Ae (ACRES)	HEADWATER NODE
1	2.60	7.30	5.004	0.20( 0.12)	0.62	0.6	100.00

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 353.80 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	3.22	5.12	6.126	0.20 ( 0.12)	0.62	0.6	110.00
2	3.39	7.30	5.004	0.20 ( 0.12)	0.62	0.8	100.00
TOTAL AREA (ACRES) =		0.77					

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 3.39 Tc (MIN.) = 7.297  
EFFECTIVE AREA (ACRES) = 0.77 AREA-AVERAGED Fm (INCH/HR) = 0.12  
AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.62  
TOTAL AREA (ACRES) = 0.77  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 353.80 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 120.00 TO NODE 121.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 33.70  
ELEVATION DATA: UPSTREAM (FEET) = 265.30 DOWNSTREAM (FEET) = 264.60

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 5.000  
\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 6.190  
SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
APARTMENTS	D	0.06	0.20	0.20	91	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.20  
SUBAREA RUNOFF (CFS) = 0.33  
TOTAL AREA (ACRES) = 0.06 PEAK FLOW RATE (CFS) = 0.33

\*\*\*\*\*

FLOW PROCESS FROM NODE 121.00 TO NODE 122.00 IS CODE = 82

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<  
>>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 171.20  
ELEVATION DATA: UPSTREAM (FEET) = 264.60 DOWNSTREAM (FEET) = 190.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 5.000  
\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 6.190  
SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL ".4 DWELLING/ACRE"	D	0.39	0.20	0.90	91	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90  
SUBAREA AREA (ACRES) = 0.39 INITIAL SUBAREA RUNOFF (CFS) = 2.11

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:  
MAINLINE Tc (MIN) = 5.00

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.190  
 SUBAREA AREA(ACRES) = 0.39 SUBAREA RUNOFF(CFS) = 2.11  
 EFFECTIVE AREA(ACRES) = 0.45 AREA-AVERAGED Fm(INCH/HR) = 0.16  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.81  
 TOTAL AREA(ACRES) = 0.45 PEAK FLOW RATE(CFS) = 2.44

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 130.00 TO NODE 131.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 68.00  
 ELEVATION DATA: UPSTREAM(FEET) = 274.30 DOWNSTREAM(FEET) = 264.50

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.190  
 SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "8-10 DWELLINGS/ACRE"	D	0.09	0.20	0.40	91	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.40  
 SUBAREA RUNOFF(CFS) = 0.49  
 TOTAL AREA(ACRES) = 0.09 PEAK FLOW RATE(CFS) = 0.49

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 131.00 TO NODE 132.00 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 262.50 DOWNSTREAM(FEET) = 254.50  
 FLOW LENGTH(FEET) = 58.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 6.0 INCH PIPE IS 2.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.37  
 GIVEN PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.49  
 PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 5.12  
 LONGEST FLOWPATH FROM NODE 130.00 TO NODE 132.00 = 126.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 132.00 TO NODE 132.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN) = 5.12  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.130  
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL ".4 DWELLING/ACRE"	D	0.09	0.20	0.90	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90  
 SUBAREA AREA(ACRES) = 0.09 SUBAREA RUNOFF(CFS) = 0.48  
 EFFECTIVE AREA(ACRES) = 0.18 AREA-AVERAGED Fm(INCH/HR) = 0.13  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.65

TOTAL AREA (ACRES) = 0.18 PEAK FLOW RATE (CFS) = 0.97

\*\*\*\*\*

FLOW PROCESS FROM NODE 132.00 TO NODE 133.00 IS CODE = 82

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<  
>>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 97.00  
ELEVATION DATA: UPSTREAM (FEET) = 254.50 DOWNSTREAM (FEET) = 225.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 5.000

\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 6.190

SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL						
".4 DWELLING/ACRE"	D	0.18	0.20	0.90	91	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90

SUBAREA AREA (ACRES) = 0.18 INITIAL SUBAREA RUNOFF (CFS) = 0.97

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:

MAINLINE Tc (MIN) = 5.12

\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 6.130

SUBAREA AREA (ACRES) = 0.18 SUBAREA RUNOFF (CFS) = 0.96

EFFECTIVE AREA (ACRES) = 0.36 AREA-AVERAGED Fm (INCH/HR) = 0.16

AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.78

TOTAL AREA (ACRES) = 0.36 PEAK FLOW RATE (CFS) = 1.94

\*\*\*\*\*

FLOW PROCESS FROM NODE 140.00 TO NODE 141.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 67.00  
ELEVATION DATA: UPSTREAM (FEET) = 265.50 DOWNSTREAM (FEET) = 264.70

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 5.070

\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 6.154

SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL						
"5-7 DWELLINGS/ACRE"	D	0.09	0.20	0.50	91	5.07

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.50

SUBAREA RUNOFF (CFS) = 0.49

TOTAL AREA (ACRES) = 0.09 PEAK FLOW RATE (CFS) = 0.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 141.00 TO NODE 142.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM (FEET) = 262.70 DOWNSTREAM (FEET) = 254.50

FLOW LENGTH(FEET) = 88.50 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 6.0 INCH PIPE IS 2.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.18  
 GIVEN PIPE DIAMETER(INCH) = 6.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.49  
 PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 5.27  
 LONGEST FLOWPATH FROM NODE 140.00 TO NODE 142.00 = 155.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 142.00 TO NODE 143.00 IS CODE = 82

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<  
 >>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 88.50  
 ELEVATION DATA: UPSTREAM(FEET) = 254.50 DOWNSTREAM(FEET) = 235.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.190

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL						
".4 DWELLING/ACRE"	D	0.17	0.20	0.90	91	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90

SUBAREA AREA(ACRES) = 0.17 INITIAL SUBAREA RUNOFF(CFS) = 0.92

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:

MAINLINE Tc(MIN) = 5.27

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.048

SUBAREA AREA(ACRES) = 0.17 SUBAREA RUNOFF(CFS) = 0.90

EFFECTIVE AREA(ACRES) = 0.26 AREA-AVERAGED Fm(INCH/HR) = 0.15

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.76

TOTAL AREA(ACRES) = 0.26 PEAK FLOW RATE(CFS) = 1.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 132.00  
 ELEVATION DATA: UPSTREAM(FEET) = 265.00 DOWNSTREAM(FEET) = 235.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.190

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL						
".4 DWELLING/ACRE"	D	0.21	0.20	0.90	91	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90

SUBAREA RUNOFF(CFS) = 1.14

TOTAL AREA(ACRES) = 0.21 PEAK FLOW RATE(CFS) = 1.14

\*\*\*\*\*

FLOW PROCESS FROM NODE 210.00 TO NODE 211.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 87.50  
ELEVATION DATA: UPSTREAM(FEET) = 251.00 DOWNSTREAM(FEET) = 216.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.190

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
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RESIDENTIAL ".4 DWELLING/ACRE"	D	0.32	0.20	0.90	91	5.00
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SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.90

SUBAREA RUNOFF(CFS) = 1.73

TOTAL AREA(ACRES) = 0.32 PEAK FLOW RATE(CFS) = 1.73

\*\*\*\*\*  
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 172.00  
ELEVATION DATA: UPSTREAM(FEET) = 265.80 DOWNSTREAM(FEET) = 251.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.190

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
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CONDOMINIUMS	D	0.19	0.20	0.35	91	5.00
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SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.35

SUBAREA RUNOFF(CFS) = 1.05

TOTAL AREA(ACRES) = 0.19 PEAK FLOW RATE(CFS) = 1.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 301.00 TO NODE 301.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE  $T_c$ (MIN) = 5.00  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.190  
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
-------------------------------	-------------------	-----------------	--------------------	--------------------	-----------

COMMERCIAL	D	0.11	0.20	0.10	91
------------	---	------	------	------	----

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.10

SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.61

EFFECTIVE AREA(ACRES) = 0.30 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.05

AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.26

TOTAL AREA(ACRES) = 0.30 PEAK FLOW RATE(CFS) = 1.66



```

*****
FLOW PROCESS FROM NODE    301.00 TO NODE    302.00 IS CODE =  41
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  249.00  DOWNSTREAM(FEET) =  247.00
FLOW LENGTH(FEET) =  101.00  MANNING'S N =  0.013
DEPTH OF FLOW IN  12.0 INCH PIPE IS  4.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  5.52
GIVEN PIPE DIAMETER(INCH) =  12.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =  1.66
PIPE TRAVEL TIME(MIN.) =  0.31  Tc(MIN.) =  5.31
LONGEST FLOWPATH FROM NODE    300.00 TO NODE    302.00 =  273.00 FEET.

*****
FLOW PROCESS FROM NODE    302.00 TO NODE    302.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
MAINLINE Tc(MIN) =  5.31
* 100 YEAR RAINFALL INTENSITY(INCH/HR) =  6.033
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp          Ap      SCS
LAND USE              GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN
COMMERCIAL            D      0.12     0.20     0.10     91
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.10
SUBAREA AREA(ACRES) =  0.12     SUBAREA RUNOFF(CFS) =  0.65
EFFECTIVE AREA(ACRES) =  0.42     AREA-AVERAGED Fm(INCH/HR) =  0.04
AREA-AVERAGED Fp(INCH/HR) =  0.20  AREA-AVERAGED Ap =  0.21
TOTAL AREA(ACRES) =  0.42     PEAK FLOW RATE(CFS) =  2.26

*****
FLOW PROCESS FROM NODE    302.00 TO NODE    303.00 IS CODE =  41
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  247.00  DOWNSTREAM(FEET) =  245.00
FLOW LENGTH(FEET) =  101.50  MANNING'S N =  0.013
DEPTH OF FLOW IN  12.0 INCH PIPE IS  5.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  5.97
GIVEN PIPE DIAMETER(INCH) =  12.00  NUMBER OF PIPES =  1
PIPE-FLOW(CFS) =  2.26
PIPE TRAVEL TIME(MIN.) =  0.28  Tc(MIN.) =  5.59
LONGEST FLOWPATH FROM NODE    300.00 TO NODE    303.00 =  374.50 FEET.

*****
FLOW PROCESS FROM NODE    303.00 TO NODE    303.00 IS CODE =  10
-----
>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<
=====

*****
FLOW PROCESS FROM NODE    310.00 TO NODE    311.00 IS CODE =  21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

```

INITIAL SUBAREA FLOW-LENGTH(FEET) = 141.00  
ELEVATION DATA: UPSTREAM(FEET) = 252.50 DOWNSTREAM(FEET) = 249.80

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$  (MIN.) = 7.489

\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 4.906

SUBAREA  $T_c$  AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
RESIDENTIAL "1 DWELLING/ACRE"	D	0.23	0.20	0.80	91	7.49

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$  (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.80  
SUBAREA RUNOFF (CFS) = 0.98  
TOTAL AREA (ACRES) = 0.23 PEAK FLOW RATE (CFS) = 0.98

\*\*\*\*\*  
FLOW PROCESS FROM NODE 311.00 TO NODE 311.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE  $T_c$  (MIN) = 7.49

\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 4.906

SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
COMMERCIAL	D	0.11	0.20	0.10	91

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$  (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.10  
SUBAREA AREA (ACRES) = 0.11 SUBAREA RUNOFF (CFS) = 0.48  
EFFECTIVE AREA (ACRES) = 0.34 AREA-AVERAGED  $F_m$  (INCH/HR) = 0.11  
AREA-AVERAGED  $F_p$  (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.57  
TOTAL AREA (ACRES) = 0.34 PEAK FLOW RATE (CFS) = 1.47

\*\*\*\*\*  
FLOW PROCESS FROM NODE 311.00 TO NODE 303.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 247.80 DOWNSTREAM(FEET) = 245.00  
FLOW LENGTH(FEET) = 26.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 8.0 INCH PIPE IS 3.5 INCHES  
PIPE-FLOW VELOCITY (FEET/SEC.) = 10.11  
GIVEN PIPE DIAMETER (INCH) = 8.00 NUMBER OF PIPES = 1  
PIPE-FLOW (CFS) = 1.47  
PIPE TRAVEL TIME (MIN.) = 0.04  $T_c$  (MIN.) = 7.53  
LONGEST FLOWPATH FROM NODE 310.00 TO NODE 303.00 = 167.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 303.00 TO NODE 303.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	$Q$ (CFS)	$T_c$ (MIN.)	Intensity (INCH/HR)	$F_p$ ( $F_m$ ) (INCH/HR)	$A_p$ (ACRES)	$A_e$ (ACRES)	HEADWATER NODE
1	1.47	7.53	4.891	0.20 (0.11)	0.57	0.3	310.00

LONGEST FLOWPATH FROM NODE 310.00 TO NODE 303.00 = 167.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.26	5.59	5.886	0.20 ( 0.04)	0.21	0.4	300.00

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 303.00 = 374.50 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	3.58	5.59	5.886	0.20 ( 0.07)	0.35	0.7	300.00
2	3.34	7.53	4.891	0.20 ( 0.07)	0.37	0.8	310.00
TOTAL AREA (ACRES) =			0.76				

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 3.58 Tc (MIN.) = 5.588  
 EFFECTIVE AREA (ACRES) = 0.67 AREA-AVERAGED Fm (INCH/HR) = 0.07  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.37  
 TOTAL AREA (ACRES) = 0.76  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 303.00 = 374.50 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 303.00 TO NODE 403.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 245.00 DOWNSTREAM (FEET) = 225.70  
 FLOW LENGTH (FEET) = 81.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.8 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 16.78  
 GIVEN PIPE DIAMETER (INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 3.58  
 PIPE TRAVEL TIME (MIN.) = 0.08 Tc (MIN.) = 5.67  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 403.00 = 455.50 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN) = 5.67  
 \* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 5.845  
 SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL ".4 DWELLING/ACRE"	D	0.05	0.20	0.90	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90  
 SUBAREA AREA (ACRES) = 0.05 SUBAREA RUNOFF (CFS) = 0.25  
 EFFECTIVE AREA (ACRES) = 0.72 AREA-AVERAGED Fm (INCH/HR) = 0.08  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.39  
 TOTAL AREA (ACRES) = 0.81 PEAK FLOW RATE (CFS) = 3.75

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 400.00 TO NODE 401.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 62.00  
ELEVATION DATA: UPSTREAM(FEET) = 275.20 DOWNSTREAM(FEET) = 273.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.000

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.190

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
COMMERCIAL	D	0.10	0.20	0.10	91	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.10

SUBAREA RUNOFF(CFS) = 0.56

TOTAL AREA(ACRES) = 0.10 PEAK FLOW RATE(CFS) = 0.56

\*\*\*\*\*

FLOW PROCESS FROM NODE 401.00 TO NODE 402.00 IS CODE = 82

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE  $T_c$ ,<<<<<  
>>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 509.00  
ELEVATION DATA: UPSTREAM(FEET) = 273.00 DOWNSTREAM(FEET) = 250.50

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 6.862

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.229

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
COMMERCIAL	D	2.03	0.20	0.10	91	6.86

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.10

SUBAREA AREA(ACRES) = 2.03 INITIAL SUBAREA RUNOFF(CFS) = 9.52

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE  $T_c$ :

MAINLINE  $T_c$ (MIN) = 5.00

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.190

SUBAREA AREA(ACRES) = 2.03 SUBAREA RUNOFF(CFS) = 11.27

EFFECTIVE AREA(ACRES) = 2.13 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.02

AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.10

TOTAL AREA(ACRES) = 2.13 PEAK FLOW RATE(CFS) = 11.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 402.00 TO NODE 403.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 243.60 DOWNSTREAM(FEET) = 225.70  
FLOW LENGTH(FEET) = 123.30 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 9.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.60

GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.83  
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 5.11  
LONGEST FLOWPATH FROM NODE 400.00 TO NODE 403.00 = 185.30 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.83	5.11	6.133	0.20( 0.02)	0.10	2.1	400.00

LONGEST FLOWPATH FROM NODE 400.00 TO NODE 403.00 = 185.30 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	3.75	5.67	5.845	0.20( 0.08)	0.39	0.7	300.00
2	3.49	7.61	4.866	0.20( 0.08)	0.41	0.8	310.00

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 403.00 = 455.50 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	15.38	5.11	6.133	0.20( 0.03)	0.17	2.8	400.00
2	15.02	5.67	5.845	0.20( 0.03)	0.17	2.9	300.00
3	12.87	7.61	4.866	0.20( 0.04)	0.18	2.9	310.00

TOTAL AREA(ACRES) = 2.94

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 15.38 Tc(MIN.) = 5.110  
EFFECTIVE AREA(ACRES) = 2.78 AREA-AVERAGED Fm(INCH/HR) = 0.03  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.17  
TOTAL AREA(ACRES) = 2.94  
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 403.00 = 455.50 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 403.00 TO NODE 404.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 225.70 DOWNSTREAM(FEET) = 209.30  
FLOW LENGTH(FEET) = 79.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 9.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 22.35  
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 15.38  
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 5.17  
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 404.00 = 534.50 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 404.00 TO NODE 502.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 211.00 DOWNSTREAM(FEET) = 210.50  
 FLOW LENGTH(FEET) = 10.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.96  
 (PIPE FLOW VELOCITY CORRESPONDING TO NORMAL-DEPTH FLOW  
 AT DEPTH = 0.82 \* DIAMETER)  
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 15.38  
 PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 5.18  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 502.00 = 544.50 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 0.00 TO NODE 0.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 502.00 TO NODE 502.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 143.00  
 ELEVATION DATA: UPSTREAM(FEET) = 263.50 DOWNSTREAM(FEET) = 252.00

$$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.869

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.741

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
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RESIDENTIAL

".4 DWELLING/ACRE"	D	0.07	0.20	0.90	91	5.87
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SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90

SUBAREA RUNOFF(CFS) = 0.35

TOTAL AREA(ACRES) = 0.07 PEAK FLOW RATE(CFS) = 0.35

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 82

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<  
 >>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 336.00  
 ELEVATION DATA: UPSTREAM(FEET) = 252.00 DOWNSTREAM(FEET) = 210.50

$$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.581

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.876

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
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RESIDENTIAL  
 ".4 DWELLING/ACRE" D 0.24 0.20 0.90 91 7.58  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.90  
 SUBAREA AREA(ACRES) = 0.24 INITIAL SUBAREA RUNOFF(CFS) = 1.01

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:  
 MAINLINE Tc(MIN) = 5.87  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.741  
 SUBAREA AREA(ACRES) = 0.24 SUBAREA RUNOFF(CFS) = 1.20  
 EFFECTIVE AREA(ACRES) = 0.31 AREA-AVERAGED Fm(INCH/HR) = 0.18  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.90  
 TOTAL AREA(ACRES) = 0.31 PEAK FLOW RATE(CFS) = 1.55

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 502.00 TO NODE 502.00 IS CODE = 11  
 -----

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<<  
 =====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	1.55	5.87	5.741	0.20( 0.18)	0.90	0.3	500.00
LONGEST FLOWPATH FROM NODE 500.00 TO NODE 502.00 = 143.00 FEET.							

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	15.38	5.18	6.095	0.20( 0.03)	0.17	2.8	400.00
2	15.02	5.74	5.807	0.20( 0.03)	0.17	2.9	300.00
3	12.87	7.69	4.844	0.20( 0.04)	0.18	2.9	310.00
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 502.00 = 544.50 FEET.							

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	16.83	5.18	6.095	0.20( 0.05)	0.23	3.1	400.00
2	16.56	5.74	5.807	0.20( 0.05)	0.24	3.2	300.00
3	16.43	5.87	5.741	0.20( 0.05)	0.24	3.2	500.00
4	14.17	7.69	4.844	0.20( 0.05)	0.25	3.2	310.00
TOTAL AREA(ACRES) = 3.25							

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.83 Tc(MIN.) = 5.185  
 EFFECTIVE AREA(ACRES) = 3.05 AREA-AVERAGED Fm(INCH/HR) = 0.05  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.24  
 TOTAL AREA(ACRES) = 3.25  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 502.00 = 544.50 FEET.  
 =====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 3.25 TC(MIN.) = 5.18  
 EFFECTIVE AREA(ACRES) = 3.05 AREA-AVERAGED Fm(INCH/HR) = 0.05  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.23  
 PEAK FLOW RATE(CFS) = 16.83

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	16.83	5.18	6.095	0.20( 0.05)	0.23	3.1	400.00

2	16.56	5.74	5.807	0.20 ( 0.05)	0.24	3.2	300.00
3	16.43	5.87	5.741	0.20 ( 0.05)	0.24	3.2	500.00
4	14.17	7.69	4.844	0.20 ( 0.05)	0.25	3.2	310.00

---

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END OF RATIONAL METHOD ANALYSIS



\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
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Ver. 15.0 Release Date: 04/01/2008 License ID 1204

Analysis prepared by:

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949-474-2330

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* 100-YEAR FREQUENCY \*  
\* AREAS A, B, AND C \*  
\* SOUTH SHORES CHURCH, DANA POINT \*  
\*\*\*\*\*

FILE NAME: SSC-A-B.DAT  
TIME/DATE OF STUDY: 13:43 02/13/2012

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 12.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- CROWN TO		STREET-CROSSFALL:			CURB GUTTER-GEOMETRIES:			MANNING FACTOR (n)	
	WIDTH (FT)	CROSSFALL (FT)	IN- SIDE	OUT- / SIDE	/PARK- WAY	HEIGHT (FT)	WIDTH (FT)	LIP (FT)		HIKE (FT)
1	30.0	20.0	0.018	0.018	0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
  2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)
- \*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

```

+-----+
| AREA - A |
+-----+

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\*\*\*\*\*  
FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21  
\*\*\*\*\*

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 240.00  
ELEVATION DATA: UPSTREAM(FEET) = 274.00 DOWNSTREAM(FEET) = 265.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.250

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.017

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
COMMERCIAL	D	0.06	0.20	0.100	91	5.25

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100

SUBAREA RUNOFF(CFS) = 0.32

TOTAL AREA(ACRES) = 0.06 PEAK FLOW RATE(CFS) = 0.32

\*\*\*\*\*

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 263.00 DOWNSTREAM(FEET) = 261.00

FLOW LENGTH(FEET) = 127.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.2 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 3.28

GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 0.32

PIPE TRAVEL TIME(MIN.) = 0.64  $T_c$ (MIN.) = 5.89

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 367.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 102.00 TO NODE 102.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE  $T_c$ (MIN.) = 5.89

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.631

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
COMMERCIAL	D	0.44	0.20	0.100	91

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100

SUBAREA AREA(ACRES) = 0.44 SUBAREA RUNOFF(CFS) = 2.22

EFFECTIVE AREA(ACRES) = 0.50 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.02

AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.10

TOTAL AREA(ACRES) = 0.5 PEAK FLOW RATE(CFS) = 2.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 102.00 TO NODE 102.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE  $T_c$ (MIN.) = 5.89

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.631

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
COMMERCIAL	D	0.12	0.20	0.100	91

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.100$   
 SUBAREA AREA (ACRES) = 0.12 SUBAREA RUNOFF (CFS) = 0.61  
 EFFECTIVE AREA (ACRES) = 0.62 AREA-AVERAGED  $F_m$  (INCH/HR) = 0.02  
 AREA-AVERAGED  $F_p$  (INCH/HR) = 0.20 AREA-AVERAGED  $A_p = 0.10$   
 TOTAL AREA (ACRES) = 0.6 PEAK FLOW RATE (CFS) = 3.13

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 261.00 DOWNSTREAM (FEET) = 259.50  
 FLOW LENGTH (FEET) = 45.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.0 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 8.05  
 GIVEN PIPE DIAMETER (INCH) = 12.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 3.13  
 PIPE TRAVEL TIME (MIN.) = 0.09  $T_c$  (MIN.) = 5.99  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 412.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE  $T_c$  (MIN.) = 5.99  
 \* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 5.580  
 SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
COMMERCIAL	D	0.05	0.20	0.100	91

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$  (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.100$   
 SUBAREA AREA (ACRES) = 0.05 SUBAREA RUNOFF (CFS) = 0.25  
 EFFECTIVE AREA (ACRES) = 0.67 AREA-AVERAGED  $F_m$  (INCH/HR) = 0.02  
 AREA-AVERAGED  $F_p$  (INCH/HR) = 0.20 AREA-AVERAGED  $A_p = 0.10$   
 TOTAL AREA (ACRES) = 0.7 PEAK FLOW RATE (CFS) = 3.35

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 82  
 -----

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE  $T_c$ ,<<<<<  
 >>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 166.00  
 ELEVATION DATA: UPSTREAM (FEET) = 275.50 DOWNSTREAM (FEET) = 265.50

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
 SUBAREA ANALYSIS USED MINIMUM  $T_c$  (MIN.) = 5.000  
 \* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 6.187  
 SUBAREA  $T_c$  AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
COMMERCIAL	D	0.16	0.20	0.100	91	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$  (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p = 0.100$   
 SUBAREA AREA (ACRES) = 0.16 INITIAL SUBAREA RUNOFF (CFS) = 0.89

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE  $T_c$ :

MAINLINE Tc(MIN.) = 5.99  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.580  
 SUBAREA AREA(ACRES) = 0.16 SUBAREA RUNOFF(CFS) = 0.80  
 EFFECTIVE AREA(ACRES) = 0.83 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 0.8 PEAK FLOW RATE(CFS) = 4.15

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 259.50 DOWNSTREAM(FEET) = 259.00  
 FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 3.23  
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 4.15  
 PIPE TRAVEL TIME(MIN.) = 1.03 Tc(MIN.) = 7.02  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 612.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 104.00 TO NODE 104.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====  
 MAINLINE Tc(MIN.) = 7.02  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.094  
 SUBAREA LOSS RATE DATA(AMC III):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.26	0.20	0.100	91
COMMERCIAL	D	0.25	0.20	0.100	91
COMMERCIAL	D	0.41	0.20	0.100	91

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 0.92 SUBAREA RUNOFF(CFS) = 4.20  
 EFFECTIVE AREA(ACRES) = 1.75 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 7.99

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 259.00 DOWNSTREAM(FEET) = 248.50  
 FLOW LENGTH(FEET) = 143.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 13.57  
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 7.99  
 PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 7.20  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 105.00 = 755.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 10  
 -----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 247.00  
ELEVATION DATA: UPSTREAM(FEET) = 277.50 DOWNSTREAM(FEET) = 269.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.403

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.919

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
COMMERCIAL	D	0.50	0.20	0.100	91	5.40

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100

SUBAREA RUNOFF(CFS) = 2.65

TOTAL AREA(ACRES) = 0.50 PEAK FLOW RATE(CFS) = 2.65

\*\*\*\*\*  
FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 263.00 DOWNSTREAM(FEET) = 255.00  
FLOW LENGTH(FEET) = 96.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.37  
GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.65  
PIPE TRAVEL TIME(MIN.) = 0.15  $T_c$ (MIN.) = 5.56  
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 343.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 203.00 TO NODE 204.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 376.00  
ELEVATION DATA: UPSTREAM(FEET) = 277.50 DOWNSTREAM(FEET) = 264.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 6.338

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.401

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
-------------------------------	-------------------	-----------------	--------------------	--------------------	-----------	-----------------

COMMERCIAL D 0.99 0.20 0.100 91 6.34  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 4.79  
 TOTAL AREA(ACRES) = 0.99 PEAK FLOW RATE(CFS) = 4.79

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 204.00 TO NODE 202.00 IS CODE = 41

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 257.00 DOWNSTREAM(FEET) = 255.00  
 FLOW LENGTH(FEET) = 72.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.29  
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 4.79  
 PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 6.48  
 LONGEST FLOWPATH FROM NODE 203.00 TO NODE 202.00 = 448.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 202.00 TO NODE 202.00 IS CODE = 11

-----  
 >>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	4.79	6.48	5.332	0.20( 0.02)	0.10	1.0	203.00

LONGEST FLOWPATH FROM NODE 203.00 TO NODE 202.00 = 448.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.65	5.56	5.824	0.20( 0.02)	0.10	0.5	200.00

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 343.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	7.15	5.56	5.824	0.20( 0.02)	0.10	1.3	200.00
2	7.22	6.48	5.332	0.20( 0.02)	0.10	1.5	203.00

TOTAL AREA(ACRES) = 1.5

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 7.22 Tc(MIN.) = 6.482  
 EFFECTIVE AREA(ACRES) = 1.49 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 1.5  
 LONGEST FLOWPATH FROM NODE 203.00 TO NODE 202.00 = 448.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 202.00 TO NODE 105.00 IS CODE = 41

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 250.00 DOWNSTREAM(FEET) = 248.50

FLOW LENGTH(FEET) = 162.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.09  
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 7.22  
 PIPE TRAVEL TIME(MIN.) = 0.44 Tc(MIN.) = 6.93  
 LONGEST FLOWPATH FROM NODE 203.00 TO NODE 105.00 = 610.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	7.15	6.00	5.573	0.20( 0.02)	0.10	1.3	200.00
2	7.22	6.93	5.134	0.20( 0.02)	0.10	1.5	203.00

LONGEST FLOWPATH FROM NODE 203.00 TO NODE 105.00 = 610.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	7.99	7.20	5.022	0.20( 0.02)	0.10	1.8	100.00

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 105.00 = 755.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	14.54	6.00	5.573	0.20( 0.02)	0.10	2.8	200.00
2	15.09	6.93	5.134	0.20( 0.02)	0.10	3.2	203.00
3	15.06	7.20	5.022	0.20( 0.02)	0.10	3.2	100.00

TOTAL AREA(ACRES) = 3.2

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 15.09 Tc(MIN.) = 6.926  
 EFFECTIVE AREA(ACRES) = 3.17 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 3.2  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 105.00 = 755.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 6.93

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.134

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.56	0.20	0.100	91
COMMERCIAL	D	0.23	0.20	0.100	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 0.79 SUBAREA RUNOFF(CFS) = 3.64

EFFECTIVE AREA(ACRES) = 3.96 AREA-AVERAGED Fm(INCH/HR) = 0.02

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10

TOTAL AREA(ACRES) = 4.0 PEAK FLOW RATE(CFS) = 18.25

```
+-----+
| ON-SITE DETENTION SYSTEM                               |
| PEAK FLOW REDUCTION FROM Q100=18.25 CFS TO Q100=6.84 CFS |
| MAXIMUM STORAGE VOLUME - 0.217 AC-FT                 |
+-----+
```

```
*****
FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 7
-----
```

```
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<
```

```
=====
USER-SPECIFIED VALUES ARE AS FOLLOWS:
TC(MIN.) = 6.96 RAINFALL INTENSITY(INCH/HR) = 5.12
EFFECTIVE AREA(ACRES) = 1.48
TOTAL AREA(ACRES) = 4.00 PEAK FLOW RATE(CFS) = 6.84
AREA-AVERAGED Fm(INCH/HR) = 0.02 AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.10
NOTE: EFFECTIVE AREA IS USED AS THE TOTAL CONTRIBUTING AREA FOR ALL
CONFLUENCE ANALYSES.
```

```
*****
FLOW PROCESS FROM NODE 106.00 TO NODE 107.00 IS CODE = 41
-----
```

```
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 245.00 DOWNSTREAM(FEET) = 244.00
FLOW LENGTH(FEET) = 47.00 MANNING'S N = 0.013
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.71
PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.84
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 7.05
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 107.00 = 802.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 41
-----
```

```
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<
```

```
=====
ELEVATION DATA: UPSTREAM(FEET) = 244.00 DOWNSTREAM(FEET) = 225.00
FLOW LENGTH(FEET) = 120.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.55
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.84
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 7.16
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 108.00 = 922.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 10
-----
```

```
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 3 <<<<<
```



```

+-----+
| AREA - B                                     |
|                                             |
+-----+

```

```

*****
FLOW PROCESS FROM NODE    400.00 TO NODE    401.00 IS CODE = 21

```

```

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>>>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

```

```

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 133.00
ELEVATION DATA: UPSTREAM(FEET) = 250.00 DOWNSTREAM(FEET) = 248.70

```

```

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.619
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.529

```

```

SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp          Ap          SCS      Tc
LAND USE              GROUP   (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
PUBLIC PARK           D       0.07    0.20      0.850     91     8.62
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA RUNOFF(CFS) = 0.27
TOTAL AREA(ACRES) = 0.07 PEAK FLOW RATE(CFS) = 0.27

```

```

*****
FLOW PROCESS FROM NODE    401.00 TO NODE    402.00 IS CODE = 41

```

```

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 247.00 DOWNSTREAM(FEET) = 245.30
FLOW LENGTH(FEET) = 168.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 2.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.64
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.27
PIPE TRAVEL TIME(MIN.) = 1.06 Tc(MIN.) = 9.68
LONGEST FLOWPATH FROM NODE 400.00 TO NODE 402.00 = 301.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE    402.00 TO NODE    402.00 IS CODE = 82

```

```

>>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<
>>>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

```

```

=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 163.00
ELEVATION DATA: UPSTREAM(FEET) = 250.00 DOWNSTREAM(FEET) = 248.40

```

```

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.969
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.737

```

```

SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp          Ap          SCS      Tc
LAND USE              GROUP   (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
SCHOOL                D       0.23    0.20      0.600     91     7.97
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.600

```

SUBAREA AREA(ACRES) = 0.23 INITIAL SUBAREA RUNOFF(CFS) = 0.96

\*\* ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:

MAINLINE Tc(MIN.) = 9.68

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.238

SUBAREA AREA(ACRES) = 0.23 SUBAREA RUNOFF(CFS) = 0.85

EFFECTIVE AREA(ACRES) = 0.30 AREA-AVERAGED Fm(INCH/HR) = 0.13

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.66

TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 1.11

\*\*\*\*\*  
FLOW PROCESS FROM NODE 402.00 TO NODE 402.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 9.68

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.238

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.11	0.20	0.100	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.42

EFFECTIVE AREA(ACRES) = 0.41 AREA-AVERAGED Fm(INCH/HR) = 0.10

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.51

TOTAL AREA(ACRES) = 0.4 PEAK FLOW RATE(CFS) = 1.53

\*\*\*\*\*  
FLOW PROCESS FROM NODE 402.00 TO NODE 403.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 245.30 DOWNSTREAM(FEET) = 243.80

FLOW LENGTH(FEET) = 144.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 12.0 INCH PIPE IS 5.5 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 4.34

GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 1.53

PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 10.23

LONGEST FLOWPATH FROM NODE 400.00 TO NODE 403.00 = 445.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 10.23

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.105

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.12	0.20	0.100	91
COMMERCIAL	D	0.11	0.20	0.100	91
COMMERCIAL	D	0.11	0.20	0.100	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 0.34 SUBAREA RUNOFF(CFS) = 1.25

EFFECTIVE AREA(ACRES) = 0.75 AREA-AVERAGED Fm(INCH/HR) = 0.06

AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.32  
TOTAL AREA (ACRES) = 0.8 PEAK FLOW RATE (CFS) = 2.73

\*\*\*\*\*  
FLOW PROCESS FROM NODE 403.00 TO NODE 108.00 IS CODE = 41

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 243.80 DOWNSTREAM(FEET) = 225.00  
FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 3.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.58  
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 2.73  
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 10.43  
LONGEST FLOWPATH FROM NODE 400.00 TO NODE 108.00 = 595.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 11

-----  
>>>>>CONFLUENCE MEMORY BANK # 3 WITH THE MAIN-STREAM MEMORY<<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.73	10.43	4.060	0.20( 0.06)	0.32	0.8	400.00

LONGEST FLOWPATH FROM NODE 400.00 TO NODE 108.00 = 595.00 FEET.

\*\* MEMORY BANK # 3 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.84	7.16	5.035	0.20( 0.02)	0.10	1.5	100.00

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 108.00 = 922.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	9.17	7.16	5.035	0.20( 0.03)	0.16	2.0	100.00
2	8.24	10.43	4.060	0.20( 0.04)	0.18	2.2	400.00

TOTAL AREA (ACRES) = 4.8

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 9.17 Tc (MIN.) = 7.164  
EFFECTIVE AREA (ACRES) = 2.00 AREA-AVERAGED Fm (INCH/HR) = 0.03  
AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.18  
TOTAL AREA (ACRES) = 4.8  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 108.00 = 922.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 108.00 TO NODE 109.00 IS CODE = 41

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
>>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 225.00 DOWNSTREAM(FEET) = 220.00  
FLOW LENGTH(FEET) = 35.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.07

GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.17  
PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 7.20  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 109.00 = 957.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 109.00 TO NODE 109.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 7.20  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.022  
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.22	0.20	0.100	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 0.22 SUBAREA RUNOFF(CFS) = 0.99  
EFFECTIVE AREA(ACRES) = 2.22 AREA-AVERAGED Fm(INCH/HR) = 0.03  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.15  
TOTAL AREA(ACRES) = 5.0 PEAK FLOW RATE(CFS) = 9.95

\*\*\*\*\*  
FLOW PROCESS FROM NODE 109.00 TO NODE 110.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 220.00 DOWNSTREAM(FEET) = 210.00  
FLOW LENGTH(FEET) = 27.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 12.0 INCH PIPE IS 5.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 26.51  
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.95  
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 7.21  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 110.00 = 984.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 12

-----  
>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

-----  
+-----+  
| AREA - C |  
| |  
+-----+

\*\*\*\*\*  
FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 170.00  
ELEVATION DATA: UPSTREAM(FEET) = 263.00 DOWNSTREAM(FEET) = 248.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 6.123

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.509

SUBAREA  $T_c$  AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN	$T_c$ (MIN.)
PUBLIC PARK	D	0.08	0.20	0.850	91	6.12

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.850

SUBAREA RUNOFF(CFS) = 0.38

TOTAL AREA(ACRES) = 0.08 PEAK FLOW RATE(CFS) = 0.38

\*\*\*\*\*  
FLOW PROCESS FROM NODE 501.00 TO NODE 110.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 248.00 DOWNSTREAM(FEET) = 210.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 292.00 CHANNEL SLOPE = 0.1301

CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 1.50

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.204

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
NATURAL FAIR COVER "CHAPARRAL, BROADLEAF"	D	0.13	0.20	1.000	95

NATURAL FAIR COVER

"CHAPARRAL, BROADLEAF" D 0.13 0.20 1.000 95

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 1.000

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 0.68

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.62

AVERAGE FLOW DEPTH(FEET) = 0.21 TRAVEL TIME(MIN.) = 0.64

$T_c$ (MIN.) = 6.76

SUBAREA AREA(ACRES) = 0.13 SUBAREA RUNOFF(CFS) = 0.59

EFFECTIVE AREA(ACRES) = 0.21 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.19

AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.94

TOTAL AREA(ACRES) = 0.2 PEAK FLOW RATE(CFS) = 0.95

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.24 FLOW VELOCITY(FEET/SEC.) = 8.14

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 110.00 = 462.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	$Q$ (CFS)	$T_c$ (MIN.)	Intensity (INCH/HR)	$F_p$ ( $F_m$ ) (INCH/HR)	$A_p$	$A_e$ (ACRES)	HEADWATER NODE
1	0.95	6.76	5.204	0.20(0.19)	0.94	0.2	500.00

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 110.00 = 462.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	9.95	7.21	5.015	0.20( 0.03)	0.15	2.2	100.00
2	8.86	10.48	4.049	0.20( 0.03)	0.17	2.5	400.00
LONGEST FLOWPATH FROM NODE				100.00 TO NODE	110.00 =	984.00 FEET.	

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	10.63	6.76	5.204	0.20( 0.04)	0.22	2.3	500.00
2	10.86	7.21	5.015	0.20( 0.04)	0.22	2.4	100.00
3	9.59	10.48	4.049	0.20( 0.05)	0.23	2.7	400.00
TOTAL AREA(ACRES) =		5.2					

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 10.86 Tc(MIN.) = 7.213  
 EFFECTIVE AREA(ACRES) = 2.43 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.22  
 TOTAL AREA(ACRES) = 5.2  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 110.00 = 984.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 5.2 TC(MIN.) = 7.21  
 EFFECTIVE AREA(ACRES) = 2.43 AREA-AVERAGED Fm(INCH/HR) = 0.04  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.220  
 PEAK FLOW RATE(CFS) = 10.86

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	10.63	6.76	5.204	0.20( 0.04)	0.22	2.3	500.00
2	10.86	7.21	5.015	0.20( 0.04)	0.22	2.4	100.00
3	9.59	10.48	4.049	0.20( 0.05)	0.23	2.7	400.00

END OF RATIONAL METHOD ANALYSIS

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
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Ver. 15.0 Release Date: 04/01/2008 License ID 1204

Analysis prepared by:

Adams-Streeter Civil Engineers, Inc.  
15 Corporate Park  
Irvine, CA 92606  
949-474-2330

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* PROPOSED CONDITION - AREA "D" (EASTERLY SLOPE) \*  
\* 100-YEAR FREQUENCY STORM \*  
\* SOUTH SHORES CHURCH, DANA POINT, CA \*  
\*\*\*\*\*

FILE NAME: SSC-D-25.DAT  
TIME/DATE OF STUDY: 10:56 09/21/2011

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 12.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF-WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN-SIDE / OUT-SIDE / PARK-WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES: LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
- (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 600.00 TO NODE 601.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 175.00  
ELEVATION DATA: UPSTREAM(FEET) = 251.00 DOWNSTREAM(FEET) = 192.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$   
SUBAREA ANALYSIS USED MINIMUM  $T_c$ (MIN.) = 5.150  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 6.083  
SUBAREA  $T_c$  AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL POOR COVER						
"CHAPARRAL, NARROWLEAF"	D	0.33	0.20	1.000	91	5.15

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000  
SUBAREA RUNOFF (CFS) = 1.75  
TOTAL AREA (ACRES) = 0.33 PEAK FLOW RATE (CFS) = 1.75

\*\*\*\*\*  
FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 54.00  
ELEVATION DATA: UPSTREAM (FEET) = 239.00 DOWNSTREAM (FEET) = 224.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 5.000

\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 6.187

SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL POOR COVER						
"CHAPARRAL, NARROWLEAF"	D	0.19	0.20	1.000	91	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000  
SUBAREA RUNOFF (CFS) = 1.02  
TOTAL AREA (ACRES) = 0.19 PEAK FLOW RATE (CFS) = 1.02

\*\*\*\*\*  
FLOW PROCESS FROM NODE 800.00 TO NODE 801.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 65.00  
ELEVATION DATA: UPSTREAM (FEET) = 244.00 DOWNSTREAM (FEET) = 219.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 5.000

\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 6.187

SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL POOR COVER						
"CHAPARRAL, NARROWLEAF"	D	0.16	0.20	1.000	91	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000  
SUBAREA RUNOFF (CFS) = 0.86  
TOTAL AREA (ACRES) = 0.16 PEAK FLOW RATE (CFS) = 0.86

END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 0.2 TC (MIN.) = 5.00  
EFFECTIVE AREA (ACRES) = 0.16 AREA-AVERAGED Fm (INCH/HR) = 0.20  
AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 1.000  
PEAK FLOW RATE (CFS) = 0.86

END OF RATIONAL METHOD ANALYSIS



## **XI. On-Site Detention Basin Calculations**

- **Detention Basin Volume & Outflow Calculations**
- **Y-Bar Calculations**
- **25-Year Frequency**
- **100-Year Frequency**

### DETENTION BASIN SIZING

CALCULATION OF DETENTION BASIN OUTLET CAPACITY THE OUTLET CONSISTS OF A RESTRICTOR PLATE PLACED ON THE TOP 9" OF A 18" RCP AT THE OUTLET OF THE DETENTION BASIN. THE BOTTOM 9-INCHES ARE OPEN AND THE CAPACITY OF THE OUTLET IS BASED UPON THE SUBMERGED ORIFICE EQUATION. THE OUTFLOW RATE FOR THE SUBMERGED ORIFICE IS BASED, IN PART, BY THE HEAD DIFFERENCE BETWEEN THE WATER SURFACES ON EACH SIDE OF THE ORIFICE OPENING.

THE SUBMERGED ORIFICE EQUATION IS:  $Q=0.63A(2G\Delta H)^{1/2}$  WHERE A IS THE OPENING AREA IN SF,  $\Delta H$  IS THE DIFFERENCE IN DEPTHS ON EACH SIDE OF THE ORIFICE OPENING (MEASURED FROM THE CENTROID OF THE ORIFICE OPENING). G IS EQUAL TO 32.2 FPS.

AREA OF 9 INCH OPENING= 0.880 SQUARE FEET

DEPTH OF WATER IN BASIN (FTS)	ASSUMED DEPTH OF FLOW AT ORIFICE (FT)	CALCULATED, Q $Q=0.63A(2G\Delta H)^{1/2}$ (FT)	BASIN OUTLET INVERT ELEVATION (FT)	PONDED WATER SURFACE ELEVATION (FT)
0.75	0.37	2.74	100	100.75
1.00	0.37	3.53	100	101.00
1.50	0.37	4.73	100	101.50
2.00	0.37	5.68	100	102.00
2.50	0.37	6.49	100	102.50
3.00	0.37	7.22	100	103.00
3.50	0.37	7.87	100	103.50
4.00	0.37	8.48	100	104.00
4.50	0.37	9.04	100	104.50
5.00	0.37	9.57	100	105.00
5.50	0.37	10.08	100	105.50
6.00	0.37	10.56	100	106.00
6.50	0.37	11.02	100	106.50
7.00	0.37	11.46	100	107.00
7.50	0.37	11.88	100	107.50
8.00	0.37	12.29	100	108.00

#### SIZE AND INVERT ELEVATIONS OF UNDERGROUND STORAGE BASIN

BASIN NO	BASIN LENGTH	BASIN WIDTH	BASIN HEIGHT	BASIN AREA (SF)	OUTLET INVERT ELEV (FT)
1	80	40	8	3200	100

VOLUME OF UNDERGROUND STORAGE BASIN

DEPTH OF WATER IN BASIN (FT)	INCREMENTAL VOLUME (CUBIC FEET)	ACCUMULATED VOLUME (CUBIC FEET)	ACCUMULATED VOLUME (ACRE-FEET)
0	0	0	0
0.75	2400	2400	0.055
1.00	800	3200	0.073
1.50	1600	4800	0.110
2.00	1600	6400	0.147
2.50	1600	8000	0.184
3.00	1600	9600	0.220
3.50	1600	11200	0.257
4.00	1600	12800	0.294
4.50	1600	14400	0.331
5.00	1600	16000	0.367
5.50	1600	17600	0.404
6.00	1600	19200	0.441
6.50	1600	20800	0.478
7.00	1600	22400	0.514
7.50	1600	24000	0.551
8.00	1600	25600	0.588

OUTFLOW RATING DATA FOR:  
 OUTFLOW WITH RESTRICTOR PLATE AT 18" DIAMETER OUTLET OF BASIN  
 SET TO CONSTRICT FLOWS WITH ONLY THE BOTTOM 0.875 FEET (10.5") OPEN.

PONDED WATER SURFACE ELEVATION (FT)	DEPTH OF FLOW AT BASIN OUTLET (FT)	ACCUMULATED VOLUME (ACRE-FEET)	OUTFLOW CFS
100	0	0.000	0
100.75	0.75	0.055	2.74
101.00	1.00	0.073	3.53
101.50	1.50	0.110	4.73
102.00	2.00	0.147	5.68
102.50	2.50	0.184	6.49
103.00	3.00	0.220	7.22
103.50	3.50	0.257	7.87
104.00	4.00	0.294	8.48
104.50	4.50	0.331	9.04
105.00	5.00	0.367	9.57
105.50	5.50	0.404	10.08
106.00	6.00	0.441	10.56
106.50	6.50	0.478	11.02

SOUTH SHORES CHURCH - DANA POINT  
CALCULATION OF LOW LOSS RATE,  $Y_{BAR}$

The low loss rate is required to perform hydrograph calculations. The low loss rate,  $Y_{BAR}$  is defined in the A38, formula (C.5) as:

$$Y_{BAR} = 1 - Y$$

Where:  $Y = \frac{(P_{24} - I_a)^2}{(P_{24} - I_a + S)P_{24}}$

$P_{24}$  = 24-hour storm rainfall

$I_a$  =  $0.2 * S$

$S = \frac{1000 - 10}{CN}$

CN is found by utilizing the Orange County Hydrology Manual Figure C-3 and Figure C-4. The AES software used to develop the peak flow rates lists the CN value for each sub-area. A composite CN value is shown on Table 1. That composite is shown herein.

$$CN = 75$$

The CN value of 75 is for AMC Condition II

AMC I is used for 2- and 5- year storm events; AMC II is used for 10-, 25- and 50- year events; AMC III is used for the 100-year event.

Table C.1 of the Orange County Hydrology Manual shows that for an AMC II CN of 75 the AMC I CN is 57 and the AMC III CN is 91

The calculated values of S are:

$(AMC\ III)\ S = \frac{1000 - 10}{CN}$		$And\ I_a = 0.2 * S$	
$= \frac{1000 - 10}{91}$	$=$	$(AMC\ III)\ I_a = 0.99 * 0.2 =$	$0.20$
$= \frac{1000 - 10}{91}$	$=$		
			$0.99$

$(AMC\ II)\ S = \frac{1000 - 10}{CN}$		$(AMC\ II)\ I_a =$	
$= \frac{1000 - 10}{75}$	$=$	$3.33 * 0.2 =$	$0.67$
$= \frac{1000 - 10}{75}$	$=$		
			$3.33$

$(AMC\ I)\ S = \frac{1000 - 10}{CN}$		$(AMC\ I)\ I_a =$	
$= \frac{1000 - 10}{57}$	$=$	$7.54 * 0.2 =$	$1.51$
$= \frac{1000 - 10}{57}$	$=$		
			$7.54$

SOUTH SHORES CHURCH - DANA POINT  
CALCULATION OF LOW LOSS RATE,  $Y_{BAR}$

$Y_{BAR} =$	1-Y	and	$Y = \frac{(P_{24}-I_a)^2}{(P_{24}-I_a+S)P_{24}}$
For 100-year event, AMC III			
	$P_{24} =$		5.63 inches per the Table B.1 from the Orange County Hydrology Manual
	$Y =$		$\frac{(5.63-0.20)^2}{(5.63-0.20+0.92)*5.63}$
	$=$		0.82
AMC III	$Y_{BAR} =$	1-Y	
	$=$		0.18
For 25-year event, AMC II			
	$P_{24} =$		4.49 inches per the Table B.1 from the Orange County Hydrology Manual
	$Y =$		$\frac{(4.49-0.67)^2}{(4.49-0.67+3.09)*4.49}$
	$=$		0.45
AMC II	$Y_{BAR} =$	1-Y	
	$=$		0.55
For 10-year event, AMC II			
	$P_{24} =$		3.68 inches per the Table B.1 from the Orange County Hydrology Manual
	$Y =$		$\frac{(3.68-0.67)^2}{(3.68-0.67+3.09)*3.68}$
	$=$		0.39
AMC II	$Y_{BAR} =$	1-Y	
	$=$		0.61
For 5-year event, AMC I			
	$P_{24} =$		3.03 inches per the Table B.1 from the Orange County Hydrology Manual
	$Y =$		$\frac{(3.03-1.51)^2}{3.03-1.51+7.18)*3.03}$
	$=$		0.08
AMC I	$Y_{BAR} =$	1-Y	
	$=$		0.92

SOUTH SHORES CHURCH - DANA POINT  
CALCULATION OF LOW LOSS RATE,  $Y_{BAR}$

For 2-year event, AMC I	$P_{24} =$	2.05 inches per the Table B.1 from the Orange County Hydrology Manual
	$Y =$	$\frac{(2.05-1.44)^2}{2.05-1.44+7.18} * 2.05$
	$=$	0.02
AMC I	$Y_{BAR} =$	1-Y
	$=$	0.98

SOUTH SHORES CHURCH - DANA POINT

WEIGHTED CN (AMC II) BASED UPON RATIONAL METHOD (AES)  
PRINTOUT FOR THE 25YEAR-YEAR PEAK FLOW RATES

SUB-AREA	AREA	CN (AMCII)	WEIGHTED CN
A-1	0.06	75	4.50
A-2	0.12	75	9.00
A-3	0.44	75	33.00
A-4	0.05	75	3.75
A-5	0.16	75	12.00
A-6	0.26	75	19.50
A-7	0.25	75	18.75
A-8	0.41	75	30.75
A-9	0.50	75	37.50
A-10	0.99	75	74.25
A-11	0.56	75	42.00
A-12	0.23	75	17.25
SUM	4.03		302.25
<b>AVERAGE</b>		<b>75.0</b>	

SOUTH SHORES CHURCH - DANA POINT

WEIGHTED CN (AMC II) BASED UPON RATIONAL METHOD (AES)  
 PRINTOUT FOR THE 25YEAR-YEAR PEAK FLOW RATES

SUB-AREA	AREA	CN (AMCII)	% Pervious	Weighted %
A-1	0.06	75	0.10	0.01
A-2	0.12	75	0.10	0.01
A-3	0.44	75	0.10	0.04
A-4	0.05	75	0.10	0.01
A-5	0.16	75	0.10	0.02
A-6	0.26	75	0.10	0.03
A-7	0.25	75	0.10	0.03
A-8	0.41	75	0.10	0.04
A-9	0.50	75	0.10	0.05
A-10	0.99	75	0.10	0.10
A-11	0.56	75	0.10	0.06
A-12	0.23	75	0.10	0.02
SUM	3.24			0.324
AVERAGE				<b>10%</b>

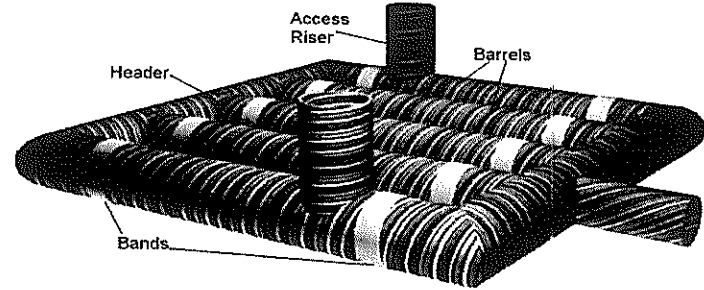


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**Project Summary**

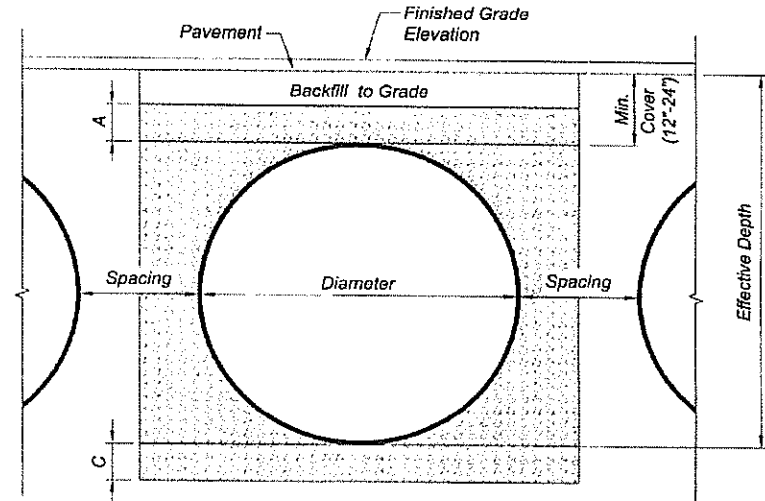
Date:	FEBRUARY 2012
Project Name:	SOUTH SHORES CHURCH
City / County:	DANA POINT, ORANGE COUNTY
State:	CA
Designed By:	NICK STREETER
Company:	ADAMS-STREETER CIVIL ENGINEERS
Telephone:	949.474.2330

Enter Information in  
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**Corrugated Metal Pipe Calculator**

Storage Volume Required (cf):	10,000
Limiting Width (ft):	20.00
Invert Depth Below Asphalt (ft):	15.00
Solid or Perforated Pipe:	Solid
Shape Or Diameter (in):	84
Number Of Headers:	2
Spacing between Barrels (ft):	3.00
Stone Width Around Perimeter of System (ft):	0
Depth A: Porous Stone Above Pipe (in):	0
Depth C: Porous Stone Below Pipe (in):	0
Stone Porosity (0 to 40%):	40

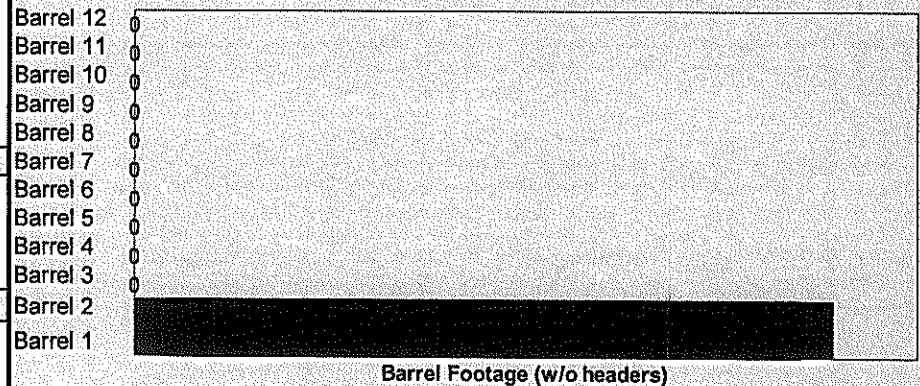
38.48 ft<sup>2</sup> Pipe Area



**System Sizing**

Pipe Storage:	10,006 cf	
Porous Stone Storage:	0 cf	
Total Storage Provided:	10,006 cf	100.1% Of Required Storage
Number of Barrels:	2 barrels	
Length per Barrel:	113.0 ft	
Length Per Header:	17.0 ft	
Rectangular Footprint (W x L):	17. ft x 127. ft	

**System Layout**



**CONTECH Materials**

Total CMP Footage:	260 ft
Approximate Total Pieces:	12 pcs
Approximate Coupling Bands:	12 bands
Approximate Truckloads:	6 trucks

**Construction Quantities\*\***

Total Excavation:	1200 cy
Porous Stone Backfill For Storage:	0 cy stone
Backfill to Grade Excluding Stone:	829 cy fill

\*\*Construction quantities are approximate and should be verified upon final design

\*\*\*\*\*

SMALL AREA UNIT HYDROGRAPH MODEL

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Ver. 15.0 Release Date: 04/01/2008 License ID 1204

Analysis prepared by:

Adams-Streeter Civil Engineers, Inc.
15 Corporate Park
Irvine, CA 92606
949-474-2330

\*\*\*\*\*

Problem Descriptions:

25-YEAR FREQUENCY
HYDROGRAPH
SOUTH SHORES CHURCH, DANA POINT

RATIONAL METHOD CALIBRATION COEFFICIENT = 0.90
TOTAL CATCHMENT AREA (ACRES) = 4.03
SOIL-LOSS RATE, Fm, (INCH/HR) = 0.020
LOW LOSS FRACTION = 0.550
TIME OF CONCENTRATION (MIN.) = 6.96
SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA
ORANGE COUNTY "VALLEY" RAINFALL VALUES ARE USED
RETURN FREQUENCY (YEARS) = 25
5-MINUTE POINT RAINFALL VALUE (INCHES) = 0.40
30-MINUTE POINT RAINFALL VALUE (INCHES) = 0.87
1-HOUR POINT RAINFALL VALUE (INCHES) = 1.15
3-HOUR POINT RAINFALL VALUE (INCHES) = 1.94
6-HOUR POINT RAINFALL VALUE (INCHES) = 2.71
24-HOUR POINT RAINFALL VALUE (INCHES) = 4.49

TOTAL CATCHMENT RUNOFF VOLUME (ACRE-FEET) = 1.20
TOTAL CATCHMENT SOIL-LOSS VOLUME (ACRE-FEET) = 0.31

\*\*\*\*\*

Table with 7 columns: TIME (HOURS), VOLUME (AF), Q (CFS), 0., 5.0, 10.0, 15.0, 20.0. Rows show data points from 0.11 to 1.38 hours.

1.50	0.0217	0.19	Q	.	.	.	.
1.62	0.0235	0.19	Q	.	.	.	.
1.73	0.0254	0.19	Q	.	.	.	.
1.85	0.0272	0.19	Q	.	.	.	.
1.96	0.0291	0.20	Q	.	.	.	.
2.08	0.0309	0.20	Q	.	.	.	.
2.20	0.0328	0.20	Q	.	.	.	.
2.31	0.0347	0.20	Q	.	.	.	.
2.43	0.0367	0.20	Q	.	.	.	.
2.54	0.0386	0.20	Q	.	.	.	.
2.66	0.0405	0.20	Q	.	.	.	.
2.78	0.0425	0.20	Q	.	.	.	.
2.89	0.0445	0.21	Q	.	.	.	.
3.01	0.0465	0.21	Q	.	.	.	.
3.12	0.0485	0.21	Q	.	.	.	.
3.24	0.0505	0.21	Q	.	.	.	.
3.36	0.0525	0.21	Q	.	.	.	.
3.47	0.0546	0.21	Q	.	.	.	.
3.59	0.0566	0.22	Q	.	.	.	.
3.70	0.0587	0.22	Q	.	.	.	.
3.82	0.0608	0.22	Q	.	.	.	.
3.94	0.0629	0.22	Q	.	.	.	.
4.05	0.0651	0.22	Q	.	.	.	.
4.17	0.0672	0.23	Q	.	.	.	.
4.28	0.0694	0.23	Q	.	.	.	.
4.40	0.0716	0.23	Q	.	.	.	.
4.52	0.0738	0.23	Q	.	.	.	.
4.63	0.0760	0.23	Q	.	.	.	.
4.75	0.0782	0.24	Q	.	.	.	.
4.86	0.0805	0.24	Q	.	.	.	.
4.98	0.0828	0.24	Q	.	.	.	.
5.10	0.0851	0.24	Q	.	.	.	.
5.21	0.0874	0.24	Q	.	.	.	.
5.33	0.0898	0.24	Q	.	.	.	.
5.44	0.0921	0.25	Q	.	.	.	.
5.56	0.0945	0.25	Q	.	.	.	.
5.68	0.0969	0.25	Q	.	.	.	.
5.79	0.0993	0.25	Q	.	.	.	.
5.91	0.1018	0.26	Q	.	.	.	.
6.02	0.1043	0.26	Q	.	.	.	.
6.14	0.1068	0.26	Q	.	.	.	.
6.26	0.1093	0.26	Q	.	.	.	.
6.37	0.1118	0.27	Q	.	.	.	.
6.49	0.1144	0.27	Q	.	.	.	.
6.60	0.1170	0.27	Q	.	.	.	.
6.72	0.1196	0.27	Q	.	.	.	.
6.84	0.1222	0.28	Q	.	.	.	.
6.95	0.1249	0.28	Q	.	.	.	.
7.07	0.1276	0.28	Q	.	.	.	.
7.18	0.1303	0.29	Q	.	.	.	.
7.30	0.1331	0.29	Q	.	.	.	.
7.42	0.1359	0.29	Q	.	.	.	.
7.53	0.1387	0.30	Q	.	.	.	.
7.65	0.1415	0.30	Q	.	.	.	.
7.76	0.1444	0.30	Q	.	.	.	.
7.88	0.1473	0.30	Q	.	.	.	.
8.00	0.1503	0.31	Q	.	.	.	.
8.11	0.1532	0.31	Q	.	.	.	.
8.23	0.1562	0.32	Q	.	.	.	.
8.34	0.1593	0.32	Q	.	.	.	.

8.46	0.1624	0.32	Q	.	.	.	.
8.58	0.1655	0.33	Q	.	.	.	.
8.69	0.1686	0.33	Q	.	.	.	.
8.81	0.1718	0.33	Q	.	.	.	.
8.92	0.1751	0.34	Q	.	.	.	.
9.04	0.1783	0.34	Q	.	.	.	.
9.16	0.1816	0.35	Q	.	.	.	.
9.27	0.1850	0.35	Q	.	.	.	.
9.39	0.1884	0.36	Q	.	.	.	.
9.50	0.1918	0.36	Q	.	.	.	.
9.62	0.1953	0.37	Q	.	.	.	.
9.74	0.1989	0.37	Q	.	.	.	.
9.85	0.2025	0.38	Q	.	.	.	.
9.97	0.2061	0.38	Q	.	.	.	.
10.08	0.2098	0.39	Q	.	.	.	.
10.20	0.2135	0.39	Q	.	.	.	.
10.32	0.2173	0.40	Q	.	.	.	.
10.43	0.2212	0.40	Q	.	.	.	.
10.55	0.2251	0.41	Q	.	.	.	.
10.66	0.2291	0.42	Q	.	.	.	.
10.78	0.2331	0.43	Q	.	.	.	.
10.90	0.2373	0.43	Q	.	.	.	.
11.01	0.2414	0.44	Q	.	.	.	.
11.13	0.2457	0.45	Q	.	.	.	.
11.24	0.2500	0.46	Q	.	.	.	.
11.36	0.2544	0.46	Q	.	.	.	.
11.48	0.2589	0.47	Q	.	.	.	.
11.59	0.2635	0.48	Q	.	.	.	.
11.71	0.2681	0.49	Q	.	.	.	.
11.82	0.2729	0.50	Q	.	.	.	.
11.94	0.2777	0.51	.Q	.	.	.	.
12.06	0.2826	0.52	.Q	.	.	.	.
12.17	0.2886	0.73	.Q	.	.	.	.
12.29	0.2956	0.74	.Q	.	.	.	.
12.40	0.3028	0.75	.Q	.	.	.	.
12.52	0.3100	0.76	.Q	.	.	.	.
12.64	0.3174	0.78	.Q	.	.	.	.
12.75	0.3250	0.79	.Q	.	.	.	.
12.87	0.3327	0.81	.Q	.	.	.	.
12.98	0.3405	0.82	.Q	.	.	.	.
13.10	0.3485	0.85	.Q	.	.	.	.
13.22	0.3567	0.86	.Q	.	.	.	.
13.33	0.3651	0.89	.Q	.	.	.	.
13.45	0.3737	0.90	.Q	.	.	.	.
13.56	0.3825	0.93	.Q	.	.	.	.
13.68	0.3915	0.95	.Q	.	.	.	.
13.80	0.4007	0.98	.Q	.	.	.	.
13.91	0.4103	1.00	. Q	.	.	.	.
14.03	0.4201	1.04	. Q	.	.	.	.
14.14	0.4301	1.05	. Q	.	.	.	.
14.26	0.4405	1.10	. Q	.	.	.	.
14.38	0.4512	1.13	. Q	.	.	.	.
14.49	0.4623	1.19	. Q	.	.	.	.
14.61	0.4738	1.22	. Q	.	.	.	.
14.72	0.4859	1.30	. Q	.	.	.	.
14.84	0.4985	1.34	. Q	.	.	.	.
14.96	0.5119	1.44	. Q	.	.	.	.
15.07	0.5259	1.50	. Q	.	.	.	.
15.19	0.5410	1.63	. Q	.	.	.	.
15.30	0.5570	1.72	. Q	.	.	.	.

15.42	0.5736	1.74	.	Q	.	.	.	.
15.54	0.5903	1.75	.	Q	.	.	.	.
15.65	0.6089	2.13	.	Q	.	.	.	.
15.77	0.6310	2.47	.	Q	.	.	.	.
15.88	0.6604	3.68	.		Q	.	.	.
16.00	0.7020	4.99	.		Q.	.	.	.
16.12	0.7947	14.36	.			Q	.	.
16.23	0.8780	3.02	.		Q	.	.	.
16.35	0.9017	1.92	.	Q	.	.	.	.
16.46	0.9196	1.82	.	Q	.	.	.	.
16.58	0.9357	1.56	.	Q	.	.	.	.
16.70	0.9499	1.39	.	Q	.	.	.	.
16.81	0.9626	1.26	.	Q	.	.	.	.
16.93	0.9741	1.16	.	Q	.	.	.	.
17.04	0.9849	1.08	.	Q	.	.	.	.
17.16	0.9949	1.02	.	Q	.	.	.	.
17.28	1.0045	0.97	.	Q	.	.	.	.
17.39	1.0135	0.92	.	Q	.	.	.	.
17.51	1.0221	0.87	.	Q	.	.	.	.
17.62	1.0303	0.84	.	Q	.	.	.	.
17.74	1.0381	0.80	.	Q	.	.	.	.
17.86	1.0456	0.77	.	Q	.	.	.	.
17.97	1.0529	0.74	.	Q	.	.	.	.
18.09	1.0597	0.67	.	Q	.	.	.	.
18.20	1.0653	0.50	.	Q	.	.	.	.
18.32	1.0700	0.49	.	Q	.	.	.	.
18.44	1.0746	0.47	.	Q	.	.	.	.
18.55	1.0790	0.45	.	Q	.	.	.	.
18.67	1.0833	0.44	.	Q	.	.	.	.
18.78	1.0874	0.42	.	Q	.	.	.	.
18.90	1.0913	0.41	.	Q	.	.	.	.
19.02	1.0952	0.40	.	Q	.	.	.	.
19.13	1.0990	0.39	.	Q	.	.	.	.
19.25	1.1026	0.37	.	Q	.	.	.	.
19.36	1.1061	0.36	.	Q	.	.	.	.
19.48	1.1096	0.35	.	Q	.	.	.	.
19.60	1.1129	0.35	.	Q	.	.	.	.
19.71	1.1162	0.34	.	Q	.	.	.	.
19.83	1.1194	0.33	.	Q	.	.	.	.
19.94	1.1225	0.32	.	Q	.	.	.	.
20.06	1.1256	0.31	.	Q	.	.	.	.
20.18	1.1285	0.31	.	Q	.	.	.	.
20.29	1.1314	0.30	.	Q	.	.	.	.
20.41	1.1343	0.29	.	Q	.	.	.	.
20.52	1.1371	0.29	.	Q	.	.	.	.
20.64	1.1398	0.28	.	Q	.	.	.	.
20.76	1.1425	0.28	.	Q	.	.	.	.
20.87	1.1451	0.27	.	Q	.	.	.	.
20.99	1.1477	0.27	.	Q	.	.	.	.
21.10	1.1502	0.26	.	Q	.	.	.	.
21.22	1.1527	0.26	.	Q	.	.	.	.
21.34	1.1551	0.25	.	Q	.	.	.	.
21.45	1.1575	0.25	.	Q	.	.	.	.
21.57	1.1598	0.24	.	Q	.	.	.	.
21.68	1.1621	0.24	.	Q	.	.	.	.
21.80	1.1644	0.23	.	Q	.	.	.	.
21.92	1.1666	0.23	.	Q	.	.	.	.
22.03	1.1688	0.23	.	Q	.	.	.	.
22.15	1.1709	0.22	.	Q	.	.	.	.
22.26	1.1730	0.22	.	Q	.	.	.	.

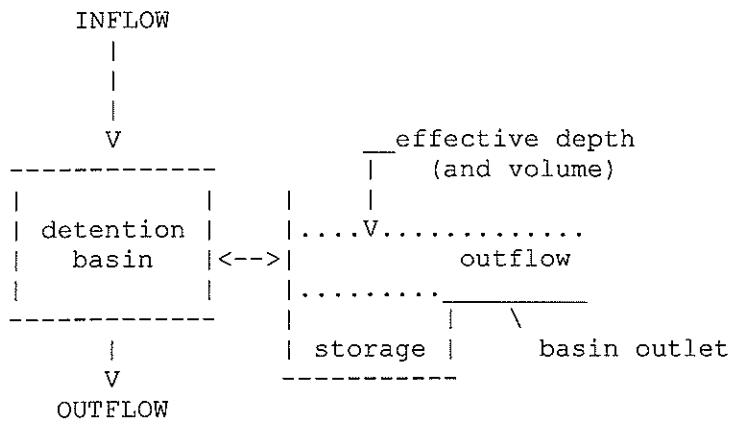
22.38	1.1751	0.22	Q	.	.	.	.
22.50	1.1772	0.21	Q	.	.	.	.
22.61	1.1792	0.21	Q	.	.	.	.
22.73	1.1812	0.21	Q	.	.	.	.
22.84	1.1831	0.20	Q	.	.	.	.
22.96	1.1851	0.20	Q	.	.	.	.
23.08	1.1870	0.20	Q	.	.	.	.
23.19	1.1889	0.19	Q	.	.	.	.
23.31	1.1907	0.19	Q	.	.	.	.
23.42	1.1925	0.19	Q	.	.	.	.
23.54	1.1943	0.19	Q	.	.	.	.
23.66	1.1961	0.18	Q	.	.	.	.
23.77	1.1978	0.18	Q	.	.	.	.
23.89	1.1996	0.18	Q	.	.	.	.
24.00	1.2013	0.18	Q	.	.	.	.
24.12	1.2021	0.00	Q	.	.	.	.

Problem Descriptions:  
 25-YEAR FREQUENCY  
 ON-SITE DETENTION SYSTEM  
 SOUTH SHORES CHURCH, DANA POINT

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FLOW-THROUGH DETENTION BASIN MODEL

SPECIFIED BASIN CONDITIONS ARE AS FOLLOWS:  
 CONSTANT HYDROGRAPH TIME UNIT (MINUTES) = 6.960  
 DEAD STORAGE (AF) = 0.00  
 SPECIFIED DEAD STORAGE (AF) FILLED = 0.00  
 ASSUMED INITIAL DEPTH (FEET) IN STORAGE BASIN = 0.00



DEPTH-VS.-STORAGE AND DEPTH-VS.-DISCHARGE INFORMATION:

TOTAL NUMBER OF BASIN DEPTH INFORMATION ENTRIES = 14

* (FEET)	* STORAGE (ACRE-FEET)	* OUTFLOW (CFS)	** (FEET)	** STORAGE (ACRE-FEET)	** OUTFLOW (CFS)
* 0.000	0.000	0.000	** 0.750	0.055	2.740*
* 1.000	0.073	3.530	** 1.500	0.110	4.730*
* 2.000	0.147	5.680	** 2.500	0.184	6.490*
* 3.000	0.220	7.220	** 3.500	0.257	7.870*
* 4.000	0.294	8.480	** 4.500	0.331	9.040*

*	5.000	0.367	9.570**	5.500	0.404	10.080*
*	6.000	0.441	10.560**	6.500	0.478	11.020*

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BASIN STORAGE, OUTFLOW AND DEPTH ROUTING VALUES:

INTERVAL NUMBER	DEPTH (FEET)	{S-O*DT/2} (ACRE-FEET)	{S+O*DT/2} (ACRE-FEET)
1	0.00	0.00000	0.00000
2	0.75	0.04187	0.06813
3	1.00	0.05608	0.08992
4	1.50	0.08733	0.13267
5	2.00	0.11977	0.17423
6	2.50	0.15289	0.21511
7	3.00	0.18539	0.25461
8	3.50	0.21928	0.29472
9	4.00	0.25335	0.33465
10	4.50	0.28767	0.37433
11	5.00	0.32113	0.41287
12	5.50	0.35568	0.45232
13	6.00	0.39038	0.49162
14	6.50	0.42518	0.53082

WHERE S=STORAGE (AF) ; O=OUTFLOW (AF/MIN.) ; DT=UNIT INTERVAL (MIN.)

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DETENTION BASIN ROUTING RESULTS:

NOTE: COMPUTED BASIN DEPTH, OUTFLOW, AND STORAGE QUANTITIES  
OCCUR AT THE GIVEN TIME. BASIN INFLOW VALUES REPRESENT THE  
AVERAGE INFLOW DURING THE RECENT HYDROGRAPH UNIT INTERVAL.

TIME (HRS)	DEAD-STORAGE FILLED (AF)	INFLOW (CFS)	EFFECTIVE DEPTH (FT)	OUTFLOW (CFS)	EFFECTIVE VOLUME (AF)
0.108	0.000	0.17	0.02	0.03	0.001
0.224	0.000	0.18	0.03	0.09	0.002
0.340	0.000	0.18	0.04	0.12	0.003
0.456	0.000	0.18	0.04	0.14	0.003
0.572	0.000	0.18	0.04	0.16	0.003
0.688	0.000	0.18	0.05	0.17	0.003
0.804	0.000	0.18	0.05	0.17	0.003
0.920	0.000	0.18	0.05	0.18	0.004
1.036	0.000	0.18	0.05	0.18	0.004
1.152	0.000	0.19	0.05	0.18	0.004
1.268	0.000	0.19	0.05	0.18	0.004
1.384	0.000	0.19	0.05	0.18	0.004
1.500	0.000	0.19	0.05	0.19	0.004
1.616	0.000	0.19	0.05	0.19	0.004
1.732	0.000	0.19	0.05	0.19	0.004
1.848	0.000	0.19	0.05	0.19	0.004
1.964	0.000	0.20	0.05	0.19	0.004
2.080	0.000	0.20	0.05	0.19	0.004
2.196	0.000	0.20	0.05	0.19	0.004
2.312	0.000	0.20	0.05	0.20	0.004
2.428	0.000	0.20	0.05	0.20	0.004
2.544	0.000	0.20	0.05	0.20	0.004
2.660	0.000	0.20	0.06	0.20	0.004
2.776	0.000	0.20	0.06	0.20	0.004
2.892	0.000	0.21	0.06	0.20	0.004
3.008	0.000	0.21	0.06	0.21	0.004
3.124	0.000	0.21	0.06	0.21	0.004
3.240	0.000	0.21	0.06	0.21	0.004
3.356	0.000	0.21	0.06	0.21	0.004
3.472	0.000	0.21	0.06	0.21	0.004

3.588	0.000	0.22	0.06	0.21	0.004
3.704	0.000	0.22	0.06	0.21	0.004
3.820	0.000	0.22	0.06	0.22	0.004
3.936	0.000	0.22	0.06	0.22	0.004
4.052	0.000	0.22	0.06	0.22	0.004
4.168	0.000	0.23	0.06	0.22	0.004
4.284	0.000	0.23	0.06	0.22	0.005
4.400	0.000	0.23	0.06	0.23	0.005
4.516	0.000	0.23	0.06	0.23	0.005
4.632	0.000	0.23	0.06	0.23	0.005
4.748	0.000	0.24	0.06	0.23	0.005
4.864	0.000	0.24	0.06	0.23	0.005
4.980	0.000	0.24	0.06	0.23	0.005
5.096	0.000	0.24	0.07	0.24	0.005
5.212	0.000	0.24	0.07	0.24	0.005
5.328	0.000	0.24	0.07	0.24	0.005
5.444	0.000	0.25	0.07	0.24	0.005
5.560	0.000	0.25	0.07	0.25	0.005
5.676	0.000	0.25	0.07	0.25	0.005
5.792	0.000	0.25	0.07	0.25	0.005
5.908	0.000	0.26	0.07	0.25	0.005
6.024	0.000	0.26	0.07	0.25	0.005
6.140	0.000	0.26	0.07	0.26	0.005
6.256	0.000	0.26	0.07	0.26	0.005
6.372	0.000	0.27	0.07	0.26	0.005
6.488	0.000	0.27	0.07	0.26	0.005
6.604	0.000	0.27	0.07	0.27	0.005
6.720	0.000	0.27	0.07	0.27	0.005
6.836	0.000	0.28	0.07	0.27	0.005
6.952	0.000	0.28	0.08	0.27	0.006
7.068	0.000	0.28	0.08	0.28	0.006
7.184	0.000	0.29	0.08	0.28	0.006
7.300	0.000	0.29	0.08	0.28	0.006
7.416	0.000	0.29	0.08	0.29	0.006
7.532	0.000	0.30	0.08	0.29	0.006
7.648	0.000	0.30	0.08	0.29	0.006
7.764	0.000	0.30	0.08	0.30	0.006
7.880	0.000	0.30	0.08	0.30	0.006
7.996	0.000	0.31	0.08	0.30	0.006
8.112	0.000	0.31	0.08	0.30	0.006
8.228	0.000	0.32	0.08	0.31	0.006
8.344	0.000	0.32	0.09	0.31	0.006
8.460	0.000	0.32	0.09	0.32	0.006
8.576	0.000	0.33	0.09	0.32	0.006
8.692	0.000	0.33	0.09	0.32	0.007
8.808	0.000	0.33	0.09	0.33	0.007
8.924	0.000	0.34	0.09	0.33	0.007
9.040	0.000	0.34	0.09	0.33	0.007
9.156	0.000	0.35	0.09	0.34	0.007
9.272	0.000	0.35	0.09	0.34	0.007
9.388	0.000	0.36	0.10	0.35	0.007
9.504	0.000	0.36	0.10	0.35	0.007
9.620	0.000	0.37	0.10	0.36	0.007
9.736	0.000	0.37	0.10	0.36	0.007
9.852	0.000	0.38	0.10	0.37	0.007
9.968	0.000	0.38	0.10	0.37	0.008
10.084	0.000	0.39	0.10	0.38	0.008
10.200	0.000	0.39	0.11	0.38	0.008
10.316	0.000	0.40	0.11	0.39	0.008
10.432	0.000	0.40	0.11	0.39	0.008



10.548	0.000	0.41	0.11	0.40	0.008
10.664	0.000	0.42	0.11	0.41	0.008
10.780	0.000	0.43	0.11	0.41	0.008
10.896	0.000	0.43	0.12	0.42	0.008
11.012	0.000	0.44	0.12	0.43	0.009
11.128	0.000	0.45	0.12	0.43	0.009
11.244	0.000	0.46	0.12	0.44	0.009
11.360	0.000	0.46	0.12	0.45	0.009
11.476	0.000	0.47	0.13	0.46	0.009
11.592	0.000	0.48	0.13	0.46	0.009
11.708	0.000	0.49	0.13	0.47	0.010
11.824	0.000	0.50	0.13	0.48	0.010
11.940	0.000	0.51	0.14	0.49	0.010
12.056	0.000	0.52	0.14	0.50	0.010
12.172	0.000	0.73	0.16	0.55	0.012
12.288	0.000	0.74	0.18	0.62	0.013
12.404	0.000	0.75	0.19	0.67	0.014
12.520	0.000	0.76	0.20	0.70	0.014
12.636	0.000	0.78	0.20	0.73	0.015
12.752	0.000	0.79	0.21	0.75	0.015
12.868	0.000	0.81	0.21	0.77	0.016
12.984	0.000	0.82	0.22	0.79	0.016
13.100	0.000	0.85	0.22	0.81	0.016
13.216	0.000	0.86	0.23	0.83	0.017
13.332	0.000	0.89	0.23	0.84	0.017
13.448	0.000	0.90	0.24	0.86	0.018
13.564	0.000	0.93	0.25	0.88	0.018
13.680	0.000	0.95	0.25	0.91	0.018
13.796	0.000	0.98	0.26	0.93	0.019
13.912	0.000	1.00	0.26	0.95	0.019
14.028	0.000	1.04	0.27	0.98	0.020
14.144	0.000	1.05	0.28	1.01	0.020
14.260	0.000	1.10	0.29	1.03	0.021
14.376	0.000	1.13	0.30	1.07	0.022
14.492	0.000	1.19	0.31	1.10	0.023
14.608	0.000	1.22	0.32	1.14	0.023
14.724	0.000	1.30	0.33	1.19	0.024
14.840	0.000	1.34	0.35	1.24	0.025
14.956	0.000	1.44	0.36	1.30	0.027
15.072	0.000	1.50	0.38	1.36	0.028
15.188	0.000	1.63	0.41	1.44	0.030
15.304	0.000	1.72	0.43	1.53	0.032
15.420	0.000	1.74	0.45	1.61	0.033
15.536	0.000	1.75	0.46	1.66	0.034
15.652	0.000	2.13	0.51	1.77	0.037
15.768	0.000	2.47	0.57	1.97	0.042
15.884	0.000	3.68	0.74	2.40	0.054
16.000	0.000	4.99	0.99	3.10	0.072
16.116	0.000	<del>4.36</del>	2.23	4.78	<del>0.164</del>
16.232	0.000	3.02	1.88	<del>5.75</del>	0.138
16.348	0.000	1.92	1.47	5.06	0.108
16.464	0.000	1.82	1.15	4.28	0.084
16.580	0.000	1.56	0.89	3.54	0.065
16.696	0.000	1.39	0.70	2.87	0.051
16.812	0.000	1.26	0.56	2.30	0.041
16.928	0.000	1.16	0.47	1.88	0.034
17.044	0.000	1.08	0.40	1.58	0.029
17.160	0.000	1.02	0.35	1.38	0.026
17.276	0.000	0.97	0.32	1.23	0.023
17.392	0.000	0.92	0.29	1.12	0.021

17.508	0.000	0.87	0.27	1.03	0.020
17.624	0.000	0.84	0.26	0.96	0.019
17.740	0.000	0.80	0.24	0.91	0.018
17.856	0.000	0.77	0.23	0.86	0.017
17.972	0.000	0.74	0.22	0.82	0.016
18.088	0.000	0.67	0.21	0.78	0.015
18.204	0.000	0.50	0.18	0.70	0.013
18.320	0.000	0.49	0.16	0.62	0.012
18.436	0.000	0.47	0.15	0.57	0.011
18.552	0.000	0.45	0.14	0.53	0.010
18.668	0.000	0.44	0.13	0.49	0.010
18.784	0.000	0.42	0.13	0.47	0.009
18.900	0.000	0.41	0.12	0.45	0.009
19.016	0.000	0.40	0.12	0.43	0.008
19.132	0.000	0.39	0.11	0.42	0.008
19.248	0.000	0.37	0.11	0.40	0.008
19.364	0.000	0.36	0.10	0.39	0.008
19.480	0.000	0.35	0.10	0.38	0.007
19.596	0.000	0.35	0.10	0.37	0.007
19.712	0.000	0.34	0.10	0.36	0.007
19.828	0.000	0.33	0.09	0.35	0.007
19.944	0.000	0.32	0.09	0.34	0.007
20.060	0.000	0.31	0.09	0.33	0.007
20.176	0.000	0.31	0.09	0.32	0.006
20.292	0.000	0.30	0.09	0.32	0.006
20.408	0.000	0.29	0.08	0.31	0.006
20.524	0.000	0.29	0.08	0.30	0.006
20.640	0.000	0.28	0.08	0.29	0.006
20.756	0.000	0.28	0.08	0.29	0.006
20.872	0.000	0.27	0.08	0.28	0.006
20.988	0.000	0.27	0.08	0.28	0.006
21.104	0.000	0.26	0.07	0.27	0.005
21.220	0.000	0.26	0.07	0.27	0.005
21.336	0.000	0.25	0.07	0.26	0.005
21.452	0.000	0.25	0.07	0.26	0.005
21.568	0.000	0.24	0.07	0.25	0.005
21.684	0.000	0.24	0.07	0.25	0.005
21.800	0.000	0.23	0.07	0.24	0.005
21.916	0.000	0.23	0.06	0.24	0.005
22.032	0.000	0.23	0.06	0.23	0.005
22.148	0.000	0.22	0.06	0.23	0.005
22.264	0.000	0.22	0.06	0.23	0.005
22.380	0.000	0.22	0.06	0.22	0.004
22.496	0.000	0.21	0.06	0.22	0.004
22.612	0.000	0.21	0.06	0.22	0.004
22.728	0.000	0.21	0.06	0.21	0.004
22.844	0.000	0.20	0.06	0.21	0.004
22.960	0.000	0.20	0.06	0.21	0.004
23.076	0.000	0.20	0.06	0.20	0.004
23.192	0.000	0.19	0.05	0.20	0.004
23.308	0.000	0.19	0.05	0.20	0.004
23.424	0.000	0.19	0.05	0.19	0.004
23.540	0.000	0.19	0.05	0.19	0.004
23.656	0.000	0.18	0.05	0.19	0.004
23.772	0.000	0.18	0.05	0.19	0.004
23.888	0.000	0.18	0.05	0.18	0.004
24.004	0.000	0.18	0.05	0.18	0.004
24.120	0.000	0.00	0.03	0.15	0.002

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SMALL AREA UNIT HYDROGRAPH MODEL

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Analysis prepared by:

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949-474-2330

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Problem Descriptions:

100-YEAR FREQUENCY  
HYDROGRAPH  
SOUTH SHORES CHURCH, DANA POINT

RATIONAL METHOD CALIBRATION COEFFICIENT = 0.90  
TOTAL CATCHMENT AREA(ACRES) = 4.06  
SOIL-LOSS RATE, Fm, (INCH/HR) = 0.020  
LOW LOSS FRACTION = 0.180  
TIME OF CONCENTRATION(MIN.) = 6.96  
SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA  
ORANGE COUNTY "VALLEY" RAINFALL VALUES ARE USED  
RETURN FREQUENCY(YEARS) = 100  
5-MINUTE POINT RAINFALL VALUE(INCHES) = 0.52  
30-MINUTE POINT RAINFALL VALUE(INCHES) = 1.09  
1-HOUR POINT RAINFALL VALUE(INCHES) = 1.45  
3-HOUR POINT RAINFALL VALUE(INCHES) = 2.43  
6-HOUR POINT RAINFALL VALUE(INCHES) = 3.36  
24-HOUR POINT RAINFALL VALUE(INCHES) = 5.63

TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 1.56  
TOTAL CATCHMENT SOIL-LOSS VOLUME(ACRE-FEET) = 0.34

\*\*\*\*\*

TIME (HOURS)	VOLUME (AF)	Q (CFS)	0.	5.0	10.0	15.0	20.0
0.11	0.0012	0.26	Q	.	.	.	.
0.22	0.0037	0.26	Q	.	.	.	.
0.34	0.0062	0.26	Q	.	.	.	.
0.46	0.0088	0.27	Q	.	.	.	.
0.57	0.0113	0.27	Q	.	.	.	.
0.69	0.0139	0.27	Q	.	.	.	.
0.80	0.0164	0.27	Q	.	.	.	.
0.92	0.0190	0.27	Q	.	.	.	.
1.04	0.0216	0.27	Q	.	.	.	.
1.15	0.0242	0.27	Q	.	.	.	.
1.27	0.0269	0.27	Q	.	.	.	.
1.38	0.0295	0.28	Q	.	.	.	.

1.50	0.0322	0.28	Q	.	.	.	.
1.62	0.0348	0.28	Q	.	.	.	.
1.73	0.0375	0.28	Q	.	.	.	.
1.85	0.0402	0.28	Q	.	.	.	.
1.96	0.0429	0.28	Q	.	.	.	.
2.08	0.0456	0.28	Q	.	.	.	.
2.20	0.0483	0.29	Q	.	.	.	.
2.31	0.0511	0.29	Q	.	.	.	.
2.43	0.0539	0.29	Q	.	.	.	.
2.54	0.0566	0.29	Q	.	.	.	.
2.66	0.0594	0.29	Q	.	.	.	.
2.78	0.0622	0.29	Q	.	.	.	.
2.89	0.0651	0.30	Q	.	.	.	.
3.01	0.0679	0.30	Q	.	.	.	.
3.12	0.0707	0.30	Q	.	.	.	.
3.24	0.0736	0.30	Q	.	.	.	.
3.36	0.0765	0.30	Q	.	.	.	.
3.47	0.0794	0.30	Q	.	.	.	.
3.59	0.0823	0.31	Q	.	.	.	.
3.70	0.0853	0.31	Q	.	.	.	.
3.82	0.0882	0.31	Q	.	.	.	.
3.94	0.0912	0.31	Q	.	.	.	.
4.05	0.0942	0.31	Q	.	.	.	.
4.17	0.0972	0.31	Q	.	.	.	.
4.28	0.1002	0.32	Q	.	.	.	.
4.40	0.1033	0.32	Q	.	.	.	.
4.52	0.1063	0.32	Q	.	.	.	.
4.63	0.1094	0.32	Q	.	.	.	.
4.75	0.1125	0.33	Q	.	.	.	.
4.86	0.1156	0.33	Q	.	.	.	.
4.98	0.1188	0.33	Q	.	.	.	.
5.10	0.1219	0.33	Q	.	.	.	.
5.21	0.1251	0.33	Q	.	.	.	.
5.33	0.1283	0.34	Q	.	.	.	.
5.44	0.1316	0.34	Q	.	.	.	.
5.56	0.1348	0.34	Q	.	.	.	.
5.68	0.1381	0.35	Q	.	.	.	.
5.79	0.1414	0.35	Q	.	.	.	.
5.91	0.1448	0.35	Q	.	.	.	.
6.02	0.1482	0.35	Q	.	.	.	.
6.14	0.1516	0.36	Q	.	.	.	.
6.26	0.1550	0.36	Q	.	.	.	.
6.37	0.1585	0.36	Q	.	.	.	.
6.49	0.1620	0.37	Q	.	.	.	.
6.60	0.1655	0.37	Q	.	.	.	.
6.72	0.1691	0.37	Q	.	.	.	.
6.84	0.1726	0.38	Q	.	.	.	.
6.95	0.1763	0.38	Q	.	.	.	.
7.07	0.1799	0.38	Q	.	.	.	.
7.18	0.1836	0.39	Q	.	.	.	.
7.30	0.1874	0.39	Q	.	.	.	.
7.42	0.1911	0.39	Q	.	.	.	.
7.53	0.1950	0.40	Q	.	.	.	.
7.65	0.1988	0.40	Q	.	.	.	.
7.76	0.2027	0.41	Q	.	.	.	.
7.88	0.2066	0.41	Q	.	.	.	.
8.00	0.2106	0.42	Q	.	.	.	.
8.11	0.2146	0.42	Q	.	.	.	.
8.23	0.2187	0.43	Q	.	.	.	.
8.34	0.2228	0.43	Q	.	.	.	.

8.46	0.2269	0.44	Q	.	.	.	.
8.58	0.2311	0.44	Q	.	.	.	.
8.69	0.2353	0.45	Q	.	.	.	.
8.81	0.2396	0.45	Q	.	.	.	.
8.92	0.2439	0.46	Q	.	.	.	.
9.04	0.2483	0.46	Q	.	.	.	.
9.16	0.2528	0.47	Q	.	.	.	.
9.27	0.2573	0.47	Q	.	.	.	.
9.39	0.2618	0.48	Q	.	.	.	.
9.50	0.2664	0.48	Q	.	.	.	.
9.62	0.2711	0.49	Q	.	.	.	.
9.74	0.2758	0.50	Q	.	.	.	.
9.85	0.2806	0.50	.Q	.	.	.	.
9.97	0.2855	0.51	.Q	.	.	.	.
10.08	0.2904	0.52	.Q	.	.	.	.
10.20	0.2954	0.52	.Q	.	.	.	.
10.32	0.3004	0.53	.Q	.	.	.	.
10.43	0.3056	0.54	.Q	.	.	.	.
10.55	0.3108	0.55	.Q	.	.	.	.
10.66	0.3161	0.55	.Q	.	.	.	.
10.78	0.3214	0.57	.Q	.	.	.	.
10.90	0.3269	0.57	.Q	.	.	.	.
11.01	0.3324	0.58	.Q	.	.	.	.
11.13	0.3381	0.59	.Q	.	.	.	.
11.24	0.3438	0.60	.Q	.	.	.	.
11.36	0.3496	0.61	.Q	.	.	.	.
11.48	0.3555	0.62	.Q	.	.	.	.
11.59	0.3615	0.63	.Q	.	.	.	.
11.71	0.3677	0.65	.Q	.	.	.	.
11.82	0.3739	0.66	.Q	.	.	.	.
11.94	0.3803	0.67	.Q	.	.	.	.
12.06	0.3868	0.68	.Q	.	.	.	.
12.17	0.3944	0.90	.Q	.	.	.	.
12.29	0.4030	0.91	.Q	.	.	.	.
12.40	0.4118	0.93	.Q	.	.	.	.
12.52	0.4207	0.94	.Q	.	.	.	.
12.64	0.4299	0.96	.Q	.	.	.	.
12.75	0.4391	0.98	.Q	.	.	.	.
12.87	0.4486	1.00	. Q	.	.	.	.
12.98	0.4583	1.02	. Q	.	.	.	.
13.10	0.4682	1.05	. Q	.	.	.	.
13.22	0.4783	1.06	. Q	.	.	.	.
13.33	0.4887	1.10	. Q	.	.	.	.
13.45	0.4992	1.11	. Q	.	.	.	.
13.56	0.5101	1.15	. Q	.	.	.	.
13.68	0.5213	1.17	. Q	.	.	.	.
13.80	0.5327	1.22	. Q	.	.	.	.
13.91	0.5445	1.24	. Q	.	.	.	.
14.03	0.5566	1.29	. Q	.	.	.	.
14.14	0.5692	1.33	. Q	.	.	.	.
14.26	0.5822	1.39	. Q	.	.	.	.
14.38	0.5957	1.42	. Q	.	.	.	.
14.49	0.6097	1.50	. Q	.	.	.	.
14.61	0.6243	1.54	. Q	.	.	.	.
14.72	0.6396	1.64	. Q	.	.	.	.
14.84	0.6555	1.69	. Q	.	.	.	.
14.96	0.6724	1.82	. Q	.	.	.	.
15.07	0.6901	1.89	. Q	.	.	.	.
15.19	0.7091	2.06	. Q	.	.	.	.
15.30	0.7294	2.17	. Q	.	.	.	.

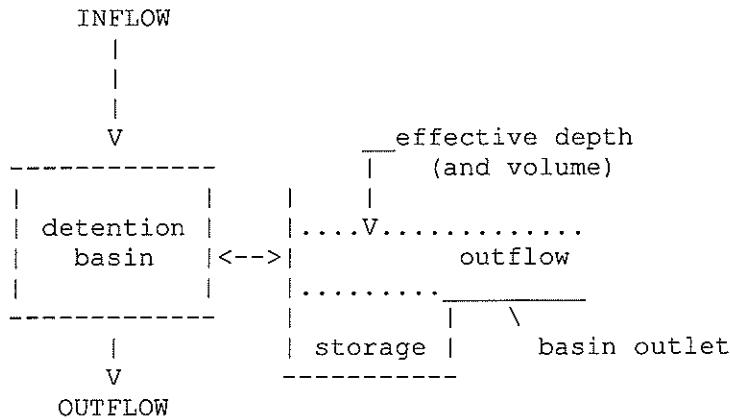
15.42	0.7506	2.24	.	Q	.	.	.	.
15.54	0.7723	2.30	.	Q	.	.	.	.
15.65	0.7966	2.77	.	Q	.	.	.	.
15.77	0.8249	3.13	.	Q	.	.	.	.
15.88	0.8614	4.49	.	Q	.	.	.	.
16.00	0.9124	6.15	.	.	Q	.	.	.
16.12	1.0316	18.70	.	.	.	.	Q	.
16.23	1.1388	3.66	.	Q	.	.	.	.
16.35	1.1683	2.50	.	Q	.	.	.	.
16.46	1.1913	2.29	.	Q	.	.	.	.
16.58	1.2118	1.97	.	Q	.	.	.	.
16.70	1.2296	1.75	.	Q	.	.	.	.
16.81	1.2456	1.59	.	Q	.	.	.	.
16.93	1.2602	1.46	.	Q	.	.	.	.
17.04	1.2737	1.36	.	Q	.	.	.	.
17.16	1.2863	1.27	.	Q	.	.	.	.
17.28	1.2981	1.19	.	Q	.	.	.	.
17.39	1.3093	1.13	.	Q	.	.	.	.
17.51	1.3199	1.08	.	Q	.	.	.	.
17.62	1.3300	1.03	.	Q	.	.	.	.
17.74	1.3397	0.99	.	Q	.	.	.	.
17.86	1.3490	0.95	.	Q	.	.	.	.
17.97	1.3579	0.92	.	Q	.	.	.	.
18.09	1.3663	0.83	.	Q	.	.	.	.
18.20	1.3735	0.66	.	Q	.	.	.	.
18.32	1.3797	0.64	.	Q	.	.	.	.
18.44	1.3858	0.62	.	Q	.	.	.	.
18.55	1.3916	0.60	.	Q	.	.	.	.
18.67	1.3972	0.58	.	Q	.	.	.	.
18.78	1.4027	0.56	.	Q	.	.	.	.
18.90	1.4080	0.54	.	Q	.	.	.	.
19.02	1.4131	0.53	.	Q	.	.	.	.
19.13	1.4181	0.51	.	Q	.	.	.	.
19.25	1.4229	0.50	Q	.	.	.	.	.
19.36	1.4277	0.49	Q	.	.	.	.	.
19.48	1.4323	0.47	Q	.	.	.	.	.
19.60	1.4368	0.46	Q	.	.	.	.	.
19.71	1.4412	0.45	Q	.	.	.	.	.
19.83	1.4454	0.44	Q	.	.	.	.	.
19.94	1.4496	0.43	Q	.	.	.	.	.
20.06	1.4537	0.42	Q	.	.	.	.	.
20.18	1.4577	0.41	Q	.	.	.	.	.
20.29	1.4617	0.41	Q	.	.	.	.	.
20.41	1.4655	0.40	Q	.	.	.	.	.
20.52	1.4693	0.39	Q	.	.	.	.	.
20.64	1.4730	0.38	Q	.	.	.	.	.
20.76	1.4766	0.37	Q	.	.	.	.	.
20.87	1.4802	0.37	Q	.	.	.	.	.
20.99	1.4837	0.36	Q	.	.	.	.	.
21.10	1.4871	0.36	Q	.	.	.	.	.
21.22	1.4905	0.35	Q	.	.	.	.	.
21.34	1.4938	0.34	Q	.	.	.	.	.
21.45	1.4971	0.34	Q	.	.	.	.	.
21.57	1.5003	0.33	Q	.	.	.	.	.
21.68	1.5034	0.33	Q	.	.	.	.	.
21.80	1.5066	0.32	Q	.	.	.	.	.
21.92	1.5097	0.32	Q	.	.	.	.	.
22.03	1.5127	0.32	Q	.	.	.	.	.
22.15	1.5157	0.31	Q	.	.	.	.	.
22.26	1.5187	0.31	Q	.	.	.	.	.

22.38	1.5216	0.30	Q	.	.	.	.
22.50	1.5245	0.30	Q	.	.	.	.
22.61	1.5274	0.30	Q	.	.	.	.
22.73	1.5302	0.29	Q	.	.	.	.
22.84	1.5330	0.29	Q	.	.	.	.
22.96	1.5358	0.29	Q	.	.	.	.
23.08	1.5386	0.29	Q	.	.	.	.
23.19	1.5413	0.28	Q	.	.	.	.
23.31	1.5440	0.28	Q	.	.	.	.
23.42	1.5466	0.28	Q	.	.	.	.
23.54	1.5493	0.27	Q	.	.	.	.
23.66	1.5519	0.27	Q	.	.	.	.
23.77	1.5545	0.27	Q	.	.	.	.
23.89	1.5570	0.27	Q	.	.	.	.
24.00	1.5596	0.26	Q	.	.	.	.
24.12	1.5608	0.00	Q	.	.	.	.

Problem Descriptions:  
 100-YEAR FREQUENCY  
 ON-SITE DETENTION SYSTEM  
 SOUTH SHORES CHURCH, DANA POINT

FLOW-THROUGH DETENTION BASIN MODEL

SPECIFIED BASIN CONDITIONS ARE AS FOLLOWS:  
 CONSTANT HYDROGRAPH TIME UNIT (MINUTES) = 6.960  
 DEAD STORAGE (AF) = 0.00  
 SPECIFIED DEAD STORAGE (AF) FILLED = 0.00  
 ASSUMED INITIAL DEPTH (FEET) IN STORAGE BASIN = 0.00



DEPTH-VS.-STORAGE AND DEPTH-VS.-DISCHARGE INFORMATION:

TOTAL NUMBER OF BASIN DEPTH INFORMATION ENTRIES = 14

* BASIN-DEPTH (FEET)	STORAGE (ACRE-FEET)	OUTFLOW (CFS)	** BASIN-DEPTH (FEET)	STORAGE (ACRE-FEET)	OUTFLOW (CFS)
* 0.000	0.000	0.000	** 0.750	0.055	2.740*
* 1.000	0.073	3.530	** 1.500	0.110	4.730*
* 2.000	0.147	5.680	** 2.500	0.184	6.490*
* 3.000	0.220	7.220	** 3.500	0.257	7.870*
* 4.000	0.294	8.480	** 4.500	0.331	9.040*

*	5.000	0.367	9.570**	5.500	0.404	10.080*
*	6.000	0.441	10.560**	6.500	0.478	11.020*

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BASIN STORAGE, OUTFLOW AND DEPTH ROUTING VALUES:

INTERVAL NUMBER	DEPTH (FEET)	{S-O*DT/2} (ACRE-FEET)	{S+O*DT/2} (ACRE-FEET)
1	0.00	0.00000	0.00000
2	0.75	0.04187	0.06813
3	1.00	0.05608	0.08992
4	1.50	0.08733	0.13267
5	2.00	0.11977	0.17423
6	2.50	0.15289	0.21511
7	3.00	0.18539	0.25461
8	3.50	0.21928	0.29472
9	4.00	0.25335	0.33465
10	4.50	0.28767	0.37433
11	5.00	0.32113	0.41287
12	5.50	0.35568	0.45232
13	6.00	0.39038	0.49162
14	6.50	0.42518	0.53082

WHERE S=STORAGE (AF) ; O=OUTFLOW (AF/MIN. ) ; DT=UNIT INTERVAL (MIN. )

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DETENTION BASIN ROUTING RESULTS:

NOTE: COMPUTED BASIN DEPTH, OUTFLOW, AND STORAGE QUANTITIES  
OCCUR AT THE GIVEN TIME. BASIN INFLOW VALUES REPRESENT THE  
AVERAGE INFLOW DURING THE RECENT HYDROGRAPH UNIT INTERVAL.

TIME (HRS)	DEAD-STORAGE FILLED (AF)	INFLOW (CFS)	EFFECTIVE DEPTH (FT)	OUTFLOW (CFS)	EFFECTIVE VOLUME (AF)
0.108	0.000	0.26	0.03	0.05	0.002
0.224	0.000	0.26	0.04	0.13	0.003
0.340	0.000	0.26	0.06	0.18	0.004
0.456	0.000	0.27	0.06	0.21	0.005
0.572	0.000	0.27	0.07	0.23	0.005
0.688	0.000	0.27	0.07	0.25	0.005
0.804	0.000	0.27	0.07	0.26	0.005
0.920	0.000	0.27	0.07	0.26	0.005
1.036	0.000	0.27	0.07	0.26	0.005
1.152	0.000	0.27	0.07	0.27	0.005
1.268	0.000	0.27	0.07	0.27	0.005
1.384	0.000	0.28	0.07	0.27	0.005
1.500	0.000	0.28	0.08	0.27	0.006
1.616	0.000	0.28	0.08	0.28	0.006
1.732	0.000	0.28	0.08	0.28	0.006
1.848	0.000	0.28	0.08	0.28	0.006
1.964	0.000	0.28	0.08	0.28	0.006
2.080	0.000	0.28	0.08	0.28	0.006
2.196	0.000	0.29	0.08	0.28	0.006
2.312	0.000	0.29	0.08	0.28	0.006
2.428	0.000	0.29	0.08	0.29	0.006
2.544	0.000	0.29	0.08	0.29	0.006
2.660	0.000	0.29	0.08	0.29	0.006
2.776	0.000	0.29	0.08	0.29	0.006
2.892	0.000	0.30	0.08	0.29	0.006
3.008	0.000	0.30	0.08	0.29	0.006
3.124	0.000	0.30	0.08	0.30	0.006
3.240	0.000	0.30	0.08	0.30	0.006
3.356	0.000	0.30	0.08	0.30	0.006
3.472	0.000	0.30	0.08	0.30	0.006



3.588	0.000	0.31	0.08	0.30	0.006
3.704	0.000	0.31	0.08	0.30	0.006
3.820	0.000	0.31	0.08	0.31	0.006
3.936	0.000	0.31	0.08	0.31	0.006
4.052	0.000	0.31	0.08	0.31	0.006
4.168	0.000	0.31	0.09	0.31	0.006
4.284	0.000	0.32	0.09	0.31	0.006
4.400	0.000	0.32	0.09	0.31	0.006
4.516	0.000	0.32	0.09	0.32	0.006
4.632	0.000	0.32	0.09	0.32	0.006
4.748	0.000	0.33	0.09	0.32	0.006
4.864	0.000	0.33	0.09	0.32	0.006
4.980	0.000	0.33	0.09	0.32	0.007
5.096	0.000	0.33	0.09	0.33	0.007
5.212	0.000	0.33	0.09	0.33	0.007
5.328	0.000	0.34	0.09	0.33	0.007
5.444	0.000	0.34	0.09	0.33	0.007
5.560	0.000	0.34	0.09	0.34	0.007
5.676	0.000	0.35	0.09	0.34	0.007
5.792	0.000	0.35	0.09	0.34	0.007
5.908	0.000	0.35	0.09	0.34	0.007
6.024	0.000	0.35	0.10	0.35	0.007
6.140	0.000	0.36	0.10	0.35	0.007
6.256	0.000	0.36	0.10	0.35	0.007
6.372	0.000	0.36	0.10	0.36	0.007
6.488	0.000	0.37	0.10	0.36	0.007
6.604	0.000	0.37	0.10	0.36	0.007
6.720	0.000	0.37	0.10	0.37	0.007
6.836	0.000	0.38	0.10	0.37	0.007
6.952	0.000	0.38	0.10	0.37	0.008
7.068	0.000	0.38	0.10	0.38	0.008
7.184	0.000	0.39	0.10	0.38	0.008
7.300	0.000	0.39	0.11	0.38	0.008
7.416	0.000	0.39	0.11	0.39	0.008
7.532	0.000	0.40	0.11	0.39	0.008
7.648	0.000	0.40	0.11	0.40	0.008
7.764	0.000	0.41	0.11	0.40	0.008
7.880	0.000	0.41	0.11	0.40	0.008
7.996	0.000	0.42	0.11	0.41	0.008
8.112	0.000	0.42	0.11	0.41	0.008
8.228	0.000	0.43	0.11	0.42	0.008
8.344	0.000	0.43	0.12	0.42	0.008
8.460	0.000	0.44	0.12	0.42	0.009
8.576	0.000	0.44	0.12	0.43	0.009
8.692	0.000	0.45	0.12	0.43	0.009
8.808	0.000	0.45	0.12	0.44	0.009
8.924	0.000	0.46	0.12	0.44	0.009
9.040	0.000	0.46	0.12	0.45	0.009
9.156	0.000	0.47	0.13	0.45	0.009
9.272	0.000	0.47	0.13	0.46	0.009
9.388	0.000	0.48	0.13	0.47	0.009
9.504	0.000	0.48	0.13	0.47	0.010
9.620	0.000	0.49	0.13	0.48	0.010
9.736	0.000	0.50	0.13	0.48	0.010
9.852	0.000	0.50	0.13	0.49	0.010
9.968	0.000	0.51	0.14	0.50	0.010
10.084	0.000	0.52	0.14	0.50	0.010
10.200	0.000	0.52	0.14	0.51	0.010
10.316	0.000	0.53	0.14	0.52	0.010
10.432	0.000	0.54	0.14	0.52	0.011

10.548	0.000	0.55	0.15	0.53	0.011
10.664	0.000	0.55	0.15	0.54	0.011
10.780	0.000	0.57	0.15	0.55	0.011
10.896	0.000	0.57	0.15	0.56	0.011
11.012	0.000	0.58	0.16	0.56	0.011
11.128	0.000	0.59	0.16	0.57	0.012
11.244	0.000	0.60	0.16	0.58	0.012
11.360	0.000	0.61	0.16	0.59	0.012
11.476	0.000	0.62	0.17	0.60	0.012
11.592	0.000	0.63	0.17	0.61	0.012
11.708	0.000	0.65	0.17	0.62	0.013
11.824	0.000	0.66	0.17	0.63	0.013
11.940	0.000	0.67	0.18	0.65	0.013
12.056	0.000	0.68	0.18	0.66	0.013
12.172	0.000	0.90	0.21	0.71	0.015
12.288	0.000	0.91	0.22	0.78	0.016
12.404	0.000	0.93	0.23	0.83	0.017
12.520	0.000	0.94	0.24	0.87	0.018
12.636	0.000	0.96	0.25	0.90	0.018
12.752	0.000	0.98	0.26	0.93	0.019
12.868	0.000	1.00	0.26	0.95	0.019
12.984	0.000	1.02	0.27	0.97	0.020
13.100	0.000	1.05	0.28	1.00	0.020
13.216	0.000	1.06	0.28	1.02	0.021
13.332	0.000	1.10	0.29	1.04	0.021
13.448	0.000	1.11	0.29	1.07	0.022
13.564	0.000	1.15	0.30	1.09	0.022
13.680	0.000	1.17	0.31	1.12	0.023
13.796	0.000	1.22	0.32	1.15	0.023
13.912	0.000	1.24	0.33	1.18	0.024
14.028	0.000	1.29	0.34	1.21	0.025
14.144	0.000	1.33	0.35	1.25	0.025
14.260	0.000	1.39	0.36	1.29	0.026
14.376	0.000	1.42	0.37	1.34	0.027
14.492	0.000	1.50	0.39	1.39	0.028
14.608	0.000	1.54	0.40	1.44	0.029
14.724	0.000	1.64	0.42	1.50	0.031
14.840	0.000	1.69	0.44	1.56	0.032
14.956	0.000	1.82	0.46	1.64	0.034
15.072	0.000	1.89	0.48	1.72	0.035
15.188	0.000	2.06	0.51	1.82	0.038
15.304	0.000	2.17	0.54	1.93	0.040
15.420	0.000	2.24	0.57	2.04	0.042
15.536	0.000	2.30	0.59	2.13	0.044
15.652	0.000	2.77	0.66	2.29	0.048
15.768	0.000	3.13	0.73	2.54	0.054
15.884	0.000	4.49	0.93	3.00	0.068
16.000	0.000	6.15	1.25	3.72	0.091
16.116	0.000	8.70	2.95	5.64	0.217
16.232	0.000	3.66	2.53	6.84	0.186
16.348	0.000	2.50	2.06	6.15	0.151
16.464	0.000	2.29	1.65	5.40	0.121
16.580	0.000	1.97	1.31	4.65	0.096
16.696	0.000	1.75	1.03	3.93	0.075
16.812	0.000	1.59	0.80	3.25	0.059
16.928	0.000	1.46	0.65	2.64	0.048
17.044	0.000	1.36	0.54	2.18	0.040
17.160	0.000	1.27	0.47	1.84	0.034
17.276	0.000	1.19	0.41	1.61	0.030
17.392	0.000	1.13	0.37	1.44	0.027

17.508	0.000	1.08	0.34	1.31	0.025
17.624	0.000	1.03	0.32	1.21	0.023
17.740	0.000	0.99	0.30	1.13	0.022
17.856	0.000	0.95	0.29	1.07	0.021
17.972	0.000	0.92	0.27	1.02	0.020
18.088	0.000	0.83	0.25	0.96	0.019
18.204	0.000	0.66	0.23	0.88	0.017
18.320	0.000	0.64	0.21	0.79	0.015
18.436	0.000	0.62	0.19	0.73	0.014
18.552	0.000	0.60	0.18	0.68	0.013
18.668	0.000	0.58	0.17	0.65	0.013
18.784	0.000	0.56	0.16	0.62	0.012
18.900	0.000	0.54	0.16	0.59	0.012
19.016	0.000	0.53	0.15	0.57	0.011
19.132	0.000	0.51	0.15	0.55	0.011
19.248	0.000	0.50	0.14	0.53	0.011
19.364	0.000	0.49	0.14	0.52	0.010
19.480	0.000	0.47	0.14	0.50	0.010
19.596	0.000	0.46	0.13	0.49	0.010
19.712	0.000	0.45	0.13	0.48	0.009
19.828	0.000	0.44	0.13	0.47	0.009
19.944	0.000	0.43	0.12	0.45	0.009
20.060	0.000	0.42	0.12	0.44	0.009
20.176	0.000	0.41	0.12	0.43	0.009
20.292	0.000	0.41	0.12	0.42	0.008
20.408	0.000	0.40	0.11	0.42	0.008
20.524	0.000	0.39	0.11	0.41	0.008
20.640	0.000	0.38	0.11	0.40	0.008
20.756	0.000	0.37	0.11	0.39	0.008
20.872	0.000	0.37	0.10	0.38	0.008
20.988	0.000	0.36	0.10	0.38	0.007
21.104	0.000	0.36	0.10	0.37	0.007
21.220	0.000	0.35	0.10	0.36	0.007
21.336	0.000	0.34	0.10	0.36	0.007
21.452	0.000	0.34	0.10	0.35	0.007
21.568	0.000	0.33	0.09	0.34	0.007
21.684	0.000	0.33	0.09	0.34	0.007
21.800	0.000	0.32	0.09	0.33	0.007
21.916	0.000	0.32	0.09	0.33	0.007
22.032	0.000	0.32	0.09	0.32	0.006
22.148	0.000	0.31	0.09	0.32	0.006
22.264	0.000	0.31	0.09	0.32	0.006
22.380	0.000	0.30	0.09	0.31	0.006
22.496	0.000	0.30	0.08	0.31	0.006
22.612	0.000	0.30	0.08	0.31	0.006
22.728	0.000	0.29	0.08	0.30	0.006
22.844	0.000	0.29	0.08	0.30	0.006
22.960	0.000	0.29	0.08	0.29	0.006
23.076	0.000	0.29	0.08	0.29	0.006
23.192	0.000	0.28	0.08	0.29	0.006
23.308	0.000	0.28	0.08	0.29	0.006
23.424	0.000	0.28	0.08	0.28	0.006
23.540	0.000	0.27	0.08	0.28	0.006
23.656	0.000	0.27	0.08	0.28	0.006
23.772	0.000	0.27	0.07	0.27	0.005
23.888	0.000	0.27	0.07	0.27	0.005
24.004	0.000	0.26	0.07	0.27	0.005
24.120	0.000	0.00	0.05	0.22	0.003

---

## **APPENDICES**

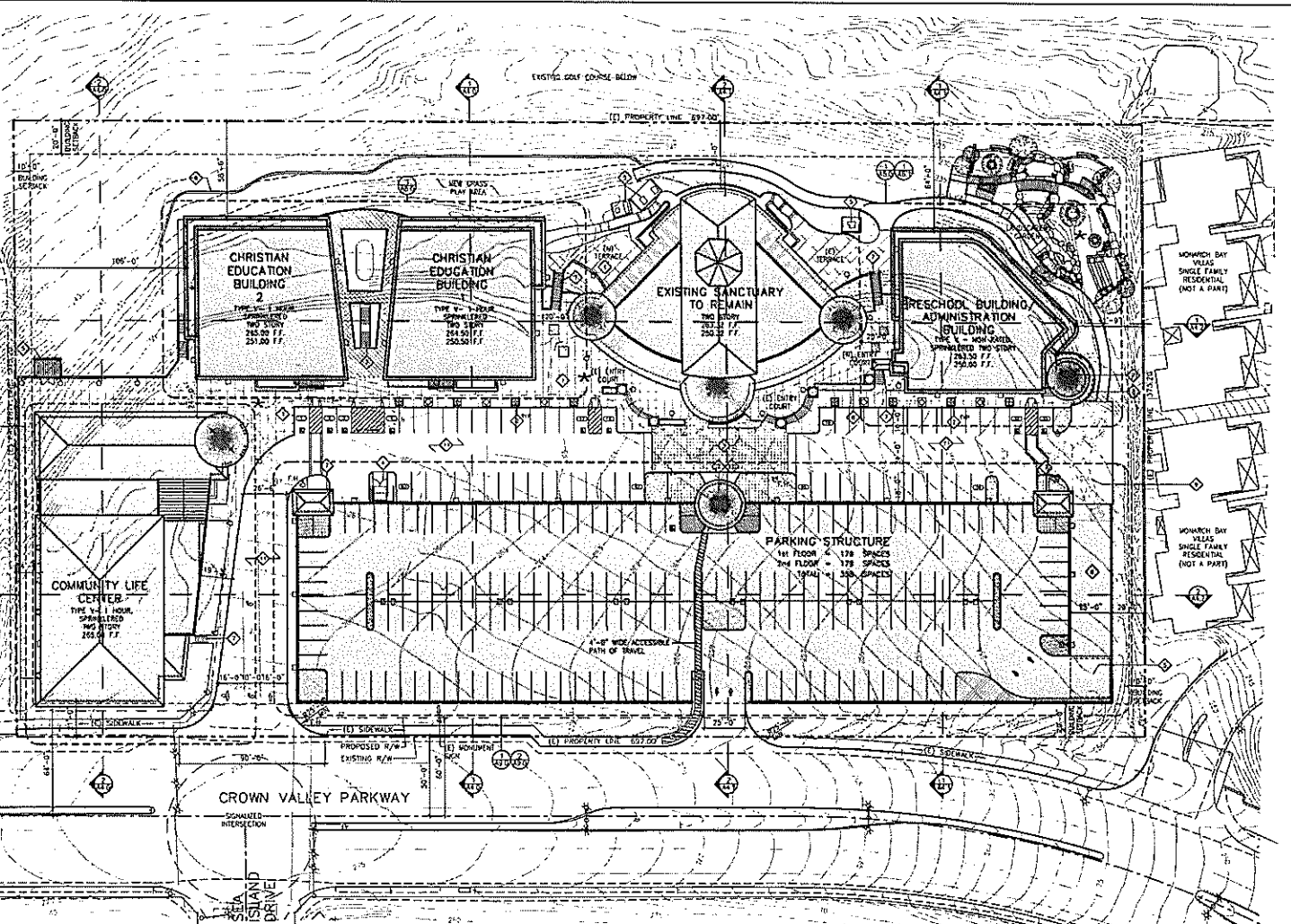
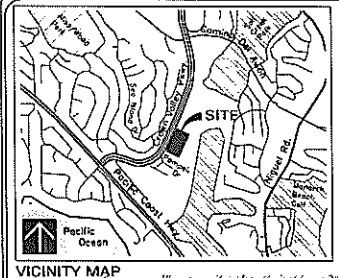
Proposed Master Site Plan

Hydrology and Hydraulic Report prepared by Boyle Engineering (1991)

Easement Agreement (for Off-Site Outlet Structure)

Hydrology Maps

- Existing Condition
- Developed Condition



- KEY NOTES**
- ◆ NEW HARDSCAPE
  - ◆ NEW TREE WELL
  - ◆ NEW ENHANCED PAVING
  - ◆ NEW CURB TRASH ENCLOSURE WITH WOOD TRELLIS
  - ◆ NEW MECHANICAL EQUIPMENT ENCLOSURE BELOW
  - ◆ NEW RETAINING WALL "SOIL RETENTION" PLANTABLE SHADING WALL SYSTEM WALL HEIGHT VARIES
  - ◆ NEW STAIRS
  - ◆ NEW RAMP
  - ◆ DCA FAN/HEADER
  - ◆ NEW ELEVATOR
  - ◆ AC PAVING

- LEGEND**
- CENTERLINE
  - - - BUILDING SETBACK
  - - - PROPERTY LINE
  - - - ACCESSIBLE PATH OF TRAVEL
  - - - RIGHT OF WAY
  - TOPOGRAPHIC OUTLINE
  - LANDSCAPED AREA
  - ▨ HARDSCAPE
  - ▭ BUILDING
  - POLE MOUNTED AREA LIGHT
  - PEDESTRIAN AREA LIGHT
  - WALL MOUNTED AREA LIGHTS, SEE SHEET A11.0 LIGHTING PLAN FOR MORE INFORMATION
  - ★ PROPOSED LOCATION OF PUBLIC ART

**PARKING COUNT**

63	ON SITE PARKING SPACES
179	SPACES 1st FLOOR PARKING STRUCTURE
178	SPACES 2nd FLOOR PARKING STRUCTURE
421	SPACES TOTAL

**BUILDING AREA**

COMMUNITY LIFE CENTER	CHRISTIAN EDUCATION BUILDING 1	BUILDING 2
1st FLR. 17,331 sf	1st FLR. 7,874 sf	1st FLR. 7,750 sf
2nd FLR. 6,083 sf	2nd FLR. 7,725 sf	2nd FLR. 7,705 sf
TOTAL: 23,414 sf	TOTAL: 15,599 sf	TOTAL: 15,455 sf

PRESCHOOL/ADMIN. BLDG.	EXISTING SANCTUARY
1st FLR. 7,737 sf	1st FLR. 9,140 sf
2nd FLR. 7,328 sf	2nd FLR. 9,238 sf
TOTAL: 15,065 sf	TOTAL: 18,378 sf

REVISIONS

07-17-07	01P	Submit 1

PLANNING DIVISION  
No. P-811  
CITY OF SAN JOSE  
OFFICE OF PLANNING

ARCH/ENG STAMP

Developed USA Permit, Submitted for:  
**South Shores Church**  
32712 Crown Valley Parkway  
Dana Point, California 92629

THE MALDEN GROUP  
**Mallock Associates, Inc.**  
180 S. HOLLYWOOD BLVD., STE. 100  
ONTARIO, CALIFORNIA 91761  
909-398-7777

DATE	ISSUE
04-05-09	01P Submit 1
3-18-11	01C WALL RFS

DRN: JRS  
21225

DRN/DATE: SL/AM

SHT. TITLE

PROPOSED MASTER SITE PLAN

SHEET NO.

**A3.0**

HYDROLOGY AND HYDRAULIC  
REPORT  
FOR  
SOUTH SHORES BAPTIST CHURCH

Prepared by:

David A. Boyle Engineering  
2098 South Grand Avenue, Suite A  
Santa Ana, California, 92705  
(714) 957-8144

January, 1991

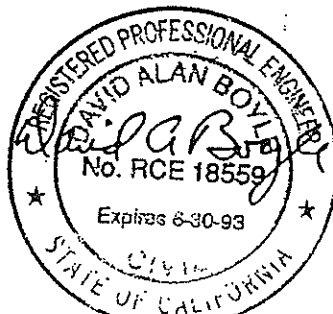


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\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 CEEMA HYDROLOGY CRITERION)  
(c) Copyright 1982-89 Advanced Engineering Software (aes)  
Ver. 5.4A Release Date: 8/21/89 Serial # 4105

Analysis prepared by:

DAVID A. BOYLE ENGINEERING  
2098 SOUTH GRAND AVE. SUITE A & B  
SANTA ANA, CA  
(714) 957-8144

-----  
FILE NAME: SS.DAT  
TIME/DATE OF STUDY: 15:13 1/10/1991  
=====

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
=====

---\*TIME-OF-CONCENTRATION MODEL\*---

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 12.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = .95  
\*DATA BANK RAINFALL USED\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 10.00 TO NODE 20.00 IS CODE = 2  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<< SUBAREA A  
=====

DEVELOPMENT IS COMMERCIAL  
TC =  $K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** .20$   
INITIAL SUBAREA FLOW-LENGTH(FEET) = 645.00  
UPSTREAM ELEVATION(FEET) = 272.20  
DOWNSTREAM ELEVATION(FEET) = 247.60  
ELEVATION DIFFERENCE(FEET) = 24.60  
TC(MIN.) =  $.304 * [(645.00 ** 3.00) / (24.60)] ** .20 = 7.770$   
100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.820  
SOIL CLASSIFICATION IS "D"  
COMMERCIAL SUBAREA LOSS RATE,  $F_m$ (INCH/HR) = .0200  
SUBAREA RUNOFF(CFS) = 8.64  
TOTAL AREA(ACRES) = 2.00 PEAK FLOW RATE(CFS) = 8.64

\*\*\*\*\*  
FLOW PROCESS FROM NODE 20.00 TO NODE 30.00 IS CODE = 3  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.9



UPSTREAM NODE ELEVATION(FEET) = 243.60  
DOWNSTREAM NODE ELEVATION(FEET) = 225.90  
FLOW LENGTH(FEET) = 123.00 MANNING'S N = .013  
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 8.64  
TRAVEL TIME(MIN.) = .11 TC(MIN.) = 7.88

\*\*\*\*\*  
FLOW PROCESS FROM NODE 30.00 TO NODE 30.00 IS CODE = 1

=====  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.88  
RAINFALL INTENSITY(INCH/HR) = 4.79  
AVERAGED Fm(INCH/HR) = .02  
EFFECTIVE STREAM AREA(ACRES) = 2.00  
TOTAL STREAM AREA(ACRES) = 2.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.64

\*\*\*\*\*  
FLOW PROCESS FROM NODE 40.00 TO NODE 30.00 IS CODE = 2

=====  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<< SUBAREA B  
=====

NATURAL POOR COVER  
TC = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\* .20  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 405.00  
UPSTREAM ELEVATION(FEET) = 266.50  
DOWNSTREAM ELEVATION(FEET) = 237.50  
ELEVATION DIFFERENCE(FEET) = 29.00  
TC(MIN.) = .525\*[( 405.00\*\* 3.00)/( 29.00)]\*\* .20 = 9.821  
100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.213  
SOIL CLASSIFICATION IS "D"  
NATURAL OR AGRICULTURE SUBAREA LOSS RATE, Fm(INCH/HR) = .2000  
SUBAREA RUNOFF(CFS) = 3.25  
TOTAL AREA(ACRES) = .90 PEAK FLOW RATE(CFS) = 3.25

\*\*\*\*\*  
FLOW PROCESS FROM NODE 30.00 TO NODE 30.00 IS CODE = 1

=====  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.82  
RAINFALL INTENSITY(INCH/HR) = 4.21  
AVERAGED Fm(INCH/HR) = .20  
EFFECTIVE STREAM AREA(ACRES) = .90  
TOTAL STREAM AREA(ACRES) = .90

PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.25

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

	Q(CFS)	Tc(MIN.)	Fm(INCH/HR)	Ae(ACRES)
1	11.62	7.88	.068	2.72
2	10.85	9.82	.076	2.90

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.62 Tc(MIN.) = 7.884  
EFFECTIVE AREA(ACRES) = 2.72 AVERAGED Fm(INCH/HR) = .07  
TOTAL AREA(ACRES) = 2.90

\*\*\*\*\*  
FLOW PROCESS FROM NODE 30.00 TO NODE 50.00 IS CODE = 3

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.9  
UPSTREAM NODE ELEVATION(FEET) = 225.60  
DOWNSTREAM NODE ELEVATION(FEET) = 208.30  
FLOW LENGTH(FEET) = 84.30 MANNING'S N = .013  
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 11.62  
TRAVEL TIME(MIN.) = .06 TC(MIN.) = 7.95

\*\*\*\*\*  
FLOW PROCESS FROM NODE 50.00 TO NODE 50.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.95  
RAINFALL INTENSITY(INCH/HR) = 4.77  
AVERAGED Fm(INCH/HR) = .07  
EFFECTIVE STREAM AREA(ACRES) = 2.72  
TOTAL STREAM AREA(ACRES) = 2.90  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.62

\*\*\*\*\*  
FLOW PROCESS FROM NODE 60.00 TO NODE 50.00 IS CODE = 2

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<< SUBAREA C

=====

NATURAL AVERAGE COVER  
TC = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\* .20  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 550.00

UPSTREAM ELEVATION(FEET) = 266.50  
 DOWNSTREAM ELEVATION(FEET) = 207.70  
 ELEVATION DIFFERENCE(FEET) = 58.80  
 $TC(MIN.) = .706 * [(550.00 * 3.00) / (58.80)] * .20 = 13.777$   
 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.476  
 SOIL CLASSIFICATION IS "D"  
 NATURAL OR AGRICULTURE SUBAREA LOSS RATE,  $F_m(INCH/HR) = .2000$   
 SUBAREA RUNOFF(CFS) = .88  
 TOTAL AREA(ACRES) = .30 PEAK FLOW RATE(CFS) = .88

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 50.00 TO NODE 50.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 13.78  
 RAINFALL INTENSITY(INCH/HR) = 3.48  
 AVERAGED  $F_m(INCH/HR) = .20$   
 EFFECTIVE STREAM AREA(ACRES) = .30  
 TOTAL STREAM AREA(ACRES) = .30  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = .88

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

	Q(CFS)	Tc(MIN.)	Fm(INCH/HR)	Ae(ACRES)
1	12.33	7.95	.076	2.90
2	11.63	9.89	.084	3.12
3	9.85	13.78	.087	3.20

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 12.33 Tc(MIN.) = 7.948  
 EFFECTIVE AREA(ACRES) = 2.90 AVERAGED  $F_m(INCH/HR) = .08$   
 TOTAL AREA(ACRES) = 3.20

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 3.20 TC(MIN.) = 7.95  
 EFFECTIVE AREA(ACRES) = 2.90 AVERAGED  $F_m(INCH/HR) = .08$   
 PEAK FLOW RATE(CFS) = 12.33

\*\*\* PEAK FLOW RATE TABLE \*\*\*

	Q(CFS)	Tc(MIN.)	Fm(INCH/HR)	Ae(ACRES)
1	12.33	7.95	.076	2.90
2	11.63	9.89	.084	3.12
3	9.85	13.78	.087	3.20

=====

END OF RATIONAL METHOD ANALYSIS

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 DCMA HYDROLOGY CRITERION)  
Copyright 1981-89 Advanced Engineering Software (aes)  
Ver. 3.4A Release Date: 3.21/85 Serial # 4105

Analysis prepared by:

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SANTA ANA, CA  
(714) 957-8144

-----  
FILE NAME: 88.DAT  
TIME/DATE OF STUDY: 15:45 1/10/1991  
=====

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

---\*TIME-OF-CONCENTRATION MODEL\*---

USER SPECIFIED STORM EVENT (YEAR) = 25.00  
SPECIFIED MINIMUM PIPE SIZE (INCH) = 12.00  
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = .95  
\*DATA BANK RAINFALL USED\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 10.00 TO NODE 20.00 IS CODE = 2

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

DEVELOPMENT IS COMMERCIAL  
TC = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\* .20  
INITIAL SUBAREA FLOW-LENGTH (FEET) = 645.00  
UPSTREAM ELEVATION (FEET) = 272.20  
DOWNSTREAM ELEVATION (FEET) = 247.60  
ELEVATION DIFFERENCE (FEET) = 24.60  
TC (MIN.) = .304\*[(645.00\*\* 3.00)/(24.60)]\*\* .20 = 7.770  
25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.768  
SOIL CLASSIFICATION IS "D"  
COMMERCIAL SUBAREA LOSS RATE, F<sub>m</sub> (INCH/HR) = .0200  
SUBAREA RUNOFF (CFS) = 6.75  
TOTAL AREA (ACRES) = 2.00 PEAK FLOW RATE (CFS) = 6.75

\*\*\*\*\*

FLOW PROCESS FROM NODE 20.00 TO NODE 30.00 IS CODE = 3

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.1 INCHES  
PIPE-FLOW VELOCITY (FEET/SEC.) = 16.9  
UPSTREAM NODE ELEVATION (FEET) = 243.60  
DOWNSTREAM NODE ELEVATION (FEET) = 225.80  
FLOW LENGTH (FEET) = 123.00 MANNING'S N = .013  
ESTIMATED PIPE DIAMETER (INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW (CFS) = 6.75  
TRAVEL TIME (MIN.) = .12 TC (MIN.) = 7.89

UPSTREAM NODE ELEVATION(FEET) = 243.50  
DOWNSTREAM NODE ELEVATION(FEET) = 225.80  
FLOW LENGTH(FEET) = 123.00 MANNING'S N = .013  
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.75  
TRAVEL TIME(MIN.) = .12 TC(MIN.) = 7.89

\*\*\*\*\*  
FLOW PROCESS FROM NODE 20.00 TO NODE 30.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.89  
RAINFALL INTENSITY(INCH/HR) = 3.74  
AVERAGED Fm(INCH/HR) = .02  
EFFECTIVE STREAM AREA(ACRES) = 2.00  
TOTAL STREAM AREA(ACRES) = 2.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.75

\*\*\*\*\*  
FLOW PROCESS FROM NODE 40.00 TO NODE 30.00 IS CODE = 2

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

NATURAL POOR COVER  
TC = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\* .20  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 405.00  
UPSTREAM ELEVATION(FEET) = 266.50  
DOWNSTREAM ELEVATION(FEET) = 237.50  
ELEVATION DIFFERENCE(FEET) = 29.00  
TC(MIN.) = .525\*[( 405.00\*\* 3.00)/( 29.00)]\*\* .20 = 9.821  
25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.301  
SOIL CLASSIFICATION IS "D"  
NATURAL OR AGRICULTURE SUBAREA LOSS RATE, Fm(INCH/HR) = .2000  
SUBAREA RUNOFF(CFS) = 2.51  
TOTAL AREA(ACRES) = .90 PEAK FLOW RATE(CFS) = 2.51

\*\*\*\*\*  
FLOW PROCESS FROM NODE 30.00 TO NODE 30.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.82  
RAINFALL INTENSITY(INCH/HR) = 3.30  
AVERAGED Fm(INCH/HR) = .20  
EFFECTIVE STREAM AREA(ACRES) = .90

PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.51

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

	Q(CFS)	Tc(MIN.)	Fm(INCH/HR)	Ae(ACRES)
1	9.05	7.89	.068	2.72
2	8.46	9.82	.076	2.90

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.05 Tc(MIN.) = 7.89  
EFFECTIVE AREA(ACRES) = 2.72 AVERAGED Fm(INCH/HR) = .07  
TOTAL AREA(ACRES) = 2.90

\*\*\*\*\*  
FLOW PROCESS FROM NODE 30.00 TO NODE 50.00 IS CODE = 3

=====  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.7  
UPSTREAM NODE ELEVATION(FEET) = 225.60  
DOWNSTREAM NODE ELEVATION(FEET) = 208.30  
FLOW LENGTH(FEET) = 84.30 MANNING'S N = .013  
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.05  
TRAVEL TIME(MIN.) = .07 TC(MIN.) = 7.96

\*\*\*\*\*  
FLOW PROCESS FROM NODE 50.00 TO NODE 50.00 IS CODE = 1

=====  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.96  
RAINFALL INTENSITY(INCH/HR) = 3.73  
AVERAGED Fm(INCH/HR) = .07  
EFFECTIVE STREAM AREA(ACRES) = 2.72  
TOTAL STREAM AREA(ACRES) = 2.90  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 60.00 TO NODE 50.00 IS CODE = 2

=====  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

NATURAL AVERAGE COVER  
TC = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\* .20  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 550.00

UPSTREAM ELEVATION(FEET) = 266.50  
 DOWNSTREAM ELEVATION(FEET) = 207.70  
 ELEVATION DIFFERENCE(FEET) = 58.80  
 $T_c(\text{MIN.}) = .705 * [ ( 550.00 + 3.00 ) / ( 58.80 ) ]^{.20} = 13.777$   
 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.727  
 SOIL CLASSIFICATION IS "D"  
 NATURAL OR AGRICULTURE SUBAREA LOSS RATE,  $F_m(\text{INCH/HR}) = .2000$   
 SUBAREA RUNOFF(CFS) = .58  
 TOTAL AREA(ACRES) = .30 PEAK FLOW RATE(CFS) = .68

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 50.00 TO NODE 50.00 IS CODE = 1  
 \*\*\*\*\*

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 13.78  
 RAINFALL INTENSITY(INCH/HR) = 2.73  
 AVERAGED  $F_m(\text{INCH/HR}) = .20$   
 EFFECTIVE STREAM AREA(ACRES) = .30  
 TOTAL STREAM AREA(ACRES) = .30  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = .68

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

	Q(CFS)	Tc(MIN.)	Fm(INCH/HR)	Ae(ACRES)
1	9.60	7.96	.076	2.90
2	9.06	9.89	.084	3.12
3	7.67	13.78	.087	3.20

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 9.60 Tc(MIN.) = 7.959  
 EFFECTIVE AREA(ACRES) = 2.90 AVERAGED  $F_m(\text{INCH/HR}) = .08$   
 TOTAL AREA(ACRES) = 3.20

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 3.20 Tc(MIN.) = 7.96  
 EFFECTIVE AREA(ACRES) = 2.90 AVERAGED  $F_m(\text{INCH/HR}) = .08$   
 PEAK FLOW RATE(CFS) = 9.60

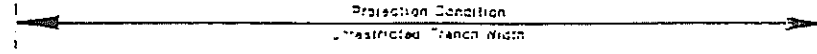
\*\*\* PEAK FLOW RATE TABLE \*\*\*

	Q(CFS)	Tc(MIN.)	Fm(INCH/HR)	Ae(ACRES)
1	9.60	7.96	.076	2.90
2	9.06	9.89	.084	3.12
3	7.67	13.78	.087	3.20

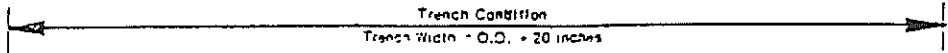
END OF RATIONAL METHOD ANALYSIS

All pipes and conduits laid parallel to the roadway shall be placed at least five (5) feet from the edge of the pavement or graded traveled roadway, unless otherwise authorized in writing by the Commissioner. The shallowest portion of any pipeline or other facility shall be installed not less than thirty (30) inches below the roadway surface. (Code 1961, § 63.0322)

PIPE SIZE	DEPTH OF COVER IN FEET										PIPE SIZE		
	1.25	1.3	1.75	2	3	4	5	7	8	10			
12	2000	2000	1500	1500	1500	1250	1250	1500	1750	2000	2250	2500	12
15	CONCRETE BACKFILL		CONCRETE BACKFILL		200				1500	1750	2000	2250	15
18					1250	1000	1000					2000	18
21		1500									1750		21
24	1250		1500			1000				1500			24
27		2000	1750						1250				27
30												1750	30
33		1750	1500								1500		33
36				1250				1000					36
39	1500	1500	1400	1300	1100				1500	1500		1900	39
42	1500	1400	1300	1200							1400		42
45	1500	1300	1200	1100	1000					1200			45
48	1200											1200	48
51		1200	1100	1000							1100		51
54	1200	1100						1000					54
57			1000										57
60				800	800	800	800	800		1100		1400	60
63				750	750			850			1250		63
66		1150	1050						850				66
69											1200	1350	69
72		1200	1100							1050			72
75				1000									75
78		1250										1200	78
81											1150		81
84			1150					800	900				84
87	400	1300								1000			87
90												1250	90
93			1200	1050	900								93
96	500	1350									1000		96
102	500												102
108		1400									1000		108



PIPE SIZE	DEPTH OF COVER IN FEET															PIPE SIZE
	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	
12	1750	1750	2000	2000	2250	2250	2250	2250	2250	2250	2250	2250	2250	2250	2250	12
15		1750	1750		2000	2000	2000	2000					2250	2250	2250	15
18	1500			1750	1750			2000	2000							18
21		1500				1750	1750			2000	2000	2000				21
24			1500					1750					2000			24
27				1500					1750					2000		27
30	1250				1500											30
33										1750						33
36		1200														36
39	1200	1300	1300	1400		1500	1600	1700	1800	1800	1900	1900	1900			39
42								1500				1800				42
45		1200								1750						45
48					1400											48
51	1100															51
54																54
57																57
60				1300			1500									60
63		1200	1250			1450			1550		1750		1850		1950	63
66																66
69																69
72								1550								72
75	1050				1300											75
78			1200													78
81														2000		81
84													1950			84
87																87
90																90
93												1900				93
96																96
102																102
108												1850				108



DATA:  
 DESIGN DENSITY = 110 pcf  
 LOAD FACTOR = 1.8  
 LIVE LOAD - H2O - S16 - 44 TRUCK

ORANGE COUNTY FLOOD CONTROL DISTRICT

D - LOAD TABLE  
 FOR REINFORCED  
 CONCRETE PIPE

1972      1 OF 1      ST-297